

1 **The linked complexity of coseismic and postseismic**
2 **faulting revealed by seismo-geodetic dynamic inversion**
3 **of the 2004 Parkfield earthquake**

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10 **Key Points:**

- 11 • We perform a joint seismo-geodetic dynamic rupture and afterslip inversion of the
12 2004 Parkfield event.
- 13 • We find that coseismic rupture is separated into a strongly radiating pulse-like and
14 a mildly radiating crack-like phase.
- 15 • Distinct dynamic rupture arrest mechanisms imprint on afterslip evolution and
16 afterslip may drive delayed aftershocks.

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Abstract

Several regularly recurring moderate-size earthquakes motivated dense instrumentation of the Parkfield section of the San Andreas fault, providing an invaluable near-fault observatory. We present a seismo-geodetic dynamic inversion of the 2004 Parkfield earthquake, which illuminates the interlinked complexity of faulting across time scales. Using fast-velocity-weakening rate-and-state friction, we jointly model 3D coseismic dynamic rupture and the 90-day evolution of postseismic slip. We utilize a parallel tempering Markov chain Monte Carlo approach to solve this non-linear high-dimensional inverse problem, constraining spatially varying prestress and fault friction parameters by 30 strong motion and 12 GPS stations. From visiting >2 million models, we discern complex coseismic rupture dynamics that transition from a strongly radiating pulse-like phase to a mildly radiating crack-like phase. Both coseismic phases are separated by a shallow strength barrier that nearly arrests rupture and leads to a gap in the afterslip. Coseismic rupture termination involves distinct arrest mechanisms that imprint on afterslip kinematics. A backward propagating afterslip front may drive delayed aftershock activity above the hypocenter. Analysis of the 10,500 best-fitting models uncovers local correlations between prestress levels and the reference friction coefficient, alongside an anticorrelation between prestress and rate-state parameters $b-a$. We find that a complex, fault-local interplay of dynamic parameters determines the nucleation, propagation, and arrest of both, co- and postseismic faulting. This study demonstrates the potential of inverse physics-based modeling to reveal novel insights and detailed characterizations of well-recorded earthquakes.

Plain Language Summary

The Parkfield section of the San Andreas plate boundary hosts regularly recurring moderate-size earthquakes. Seismic ground motions and slow deformation following the 2004 Parkfield earthquake were recorded by more than 30 seismometers and 13 GPS stations. While this is arguably one of the best-recorded earthquakes, it remains challenging to constrain the physics and properties at depth governing the earthquake from surface observations. Data-driven earthquake models solving inverse problems usually describe the kinematics of rupture. Here, we employ an expensive numerical algorithm to invert observations dynamically and find a physics-based set of parameters that simultaneously explain the earthquake and its afterslip, slow deformation following an earth-

49 quake. We find two separate phases of the earthquake that cause a similar amount of
 50 permanent displacement, but the rapid rupture of the first phase radiates much more
 51 potentially damaging seismic waves. The permanent displacement caused by the after-
 52 slip of the 2004 Parkfield earthquake exceeded its coseismic displacement. The local fric-
 53 tional properties that arrest the earthquake imprint on the subsequent afterslip evolu-
 54 tion. Our approach illustrates that physics-based models utilizing modern computing
 55 techniques can reveal new insights and unprecedented detail even of well-studied events.

56 **1 Introduction**

57 The Parkfield section marks the transition between a locked part of the main strand
 58 of the San Andreas Fault (SAF) system and a creeping section to the northwest, with
 59 slip rates of 25–30 mm/yr (Titus et al., 2005; Tong et al., 2013). The transition between
 60 the creeping and locked sections is approximately at Middle Mountain (Murray & Lang-
 61 bein, 2006). Several earthquakes of $M_w \approx 6$ struck the Parkfield section in 1857, 1881,
 62 1901, 1922, 1934, and 1966, corresponding to an average recurrence time of 22 ± 3 years
 63 (Bakun & McEvilly, 1984). The Parkfield earthquake prediction experiment (Bakun &
 64 Lindh, 1985) anticipated another $M_w \approx 6$ earthquake in 1988 ± 5 years and motivated
 65 dense seismic and geodetic instrumentation in the area. However, the anticipated Park-
 66 field earthquake only happened in 2004 without noticeable short-term precursory sig-
 67 nals (Bakun et al., 2005; Bilham, 2005). More than 40 strong-motion instruments and
 68 13 GPS stations (Fig. 1) recorded the 2004 Parkfield earthquake and its afterslip with
 69 an epicentral distance of less than 32 km (e.g., Liu et al., 2006; Johnson et al., 2006).

70 **1.1 Kinematic source inversion and back-projection imaging**

71 Kinematic source inversions and back-projection studies of the 2004 Parkfield earth-
 72 quake reveal a heterogeneous rupture process regarding slip, rupture speed, and rise time.
 73 The inferred kinematic models generally agree that the rupture process was complex de-
 74 spite its moderate size, with coseismic slip mainly confined within a depth of 4–10 km
 75 (e.g., Langbein et al., 2006). Most models suggest a primary high slip patch surround-
 76 ing the hypocenter and a second major slip area, 15–20 km northwest of the hypocen-
 77 ter (Johanson et al., 2006; Liu et al., 2006; Custódio et al., 2009; Twardzik et al., 2012),
 78 with purely geodetic models being generally smoother (Kim & Dreger, 2008; Page et al.,
 79 2009). Some studies (Fletcher et al., 2006; Custódio et al., 2009) concluded that there

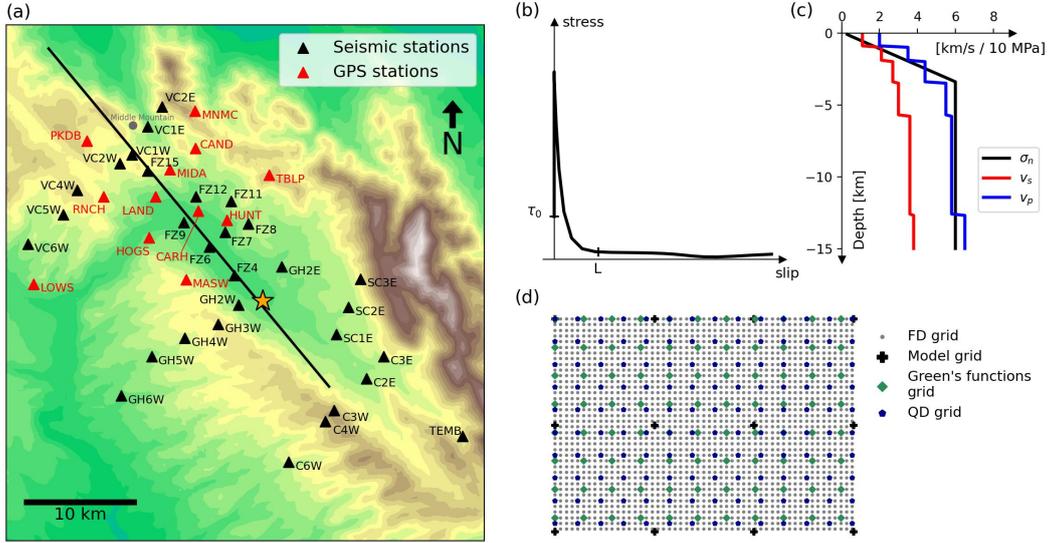


Figure 1. (a) Map view of the model domain with near-fault stations utilized in the dynamic inversion. Black triangles show seismic stations, red triangles are GPS stations, the black line is the fault trace, and the star marks the epicenter location. Topography is shown for regional context but is not accounted for in our forward models. (b) Exemplary stress evolution during coseismic dynamic rupture governed by the fast-velocity-weakening rate-and-state friction law measured in one of our dynamic rupture simulations. τ_0 represents the prestress and L the characteristic slip distance over which the frictional resistance drops from its static to its dynamic value. (c) Assumed depth-dependent normal stress σ_n and averaged seismic velocity profile used in the finite difference solver. We use two different seismic velocity profiles to compute different Green's functions for each side of the fault, respectively, following (Custódio et al., 2005). (d) Illustration of the four different grids discretizing the fault plane used in the dynamic source inversion. Dynamic model parameters are defined on the coarsest grid (model grid, black crosses) and bilinearly interpolated on the finest grid used in the finite-difference dynamic rupture solver (FD grid, grey dots) and the grid used in the quasi-dynamic boundary element method (QD grid, blue dots). Slip rates and slip from the FD or QD grids are averaged on the Green's functions grid (green dots) to compute synthetic seismograms and GPS displacements.

80 was rapid rupture onset with rupture velocities close to the S-wave speed (≈ 3.6 km/s
 81 at hypocentral depth) and rise times shorter than 1 s. Propagating to the northwest, rup-
 82 ture speed may have decreased and rise times increased (Fletcher et al., 2006; Ma et al.,
 83 2008; Custódio et al., 2009).

84 Data-driven, kinematic earthquake models use various datasets to illuminate the
 85 space-time evolution of both coseismic rupture and afterslip. Still, they typically can-
 86 not probe dynamically consistent pre-, co-, and post-seismic mechanical conditions of fault-
 87 ing. Dynamic rupture forward modeling, on the other hand, is typically limited to the
 88 coseismic timescale and compares simulation results retrospectively to observational data
 89 or kinematic models (e.g., Ulrich et al., 2019; Tinti et al., 2021; Taufiqurrahman et al.,
 90 2023; Wen et al., 2024).

91 1.2 Results from previous dynamic modeling

92 Several studies investigated the dynamic source process of the 2004 Parkfield earth-
 93 quake. Ma et al. (2008) constructed a dynamic rupture forward model using a linear slip-
 94 weakening friction law with mostly uniform frictional properties and a constant seismic
 95 S parameter (Andrews, 1976) for regions with a positive stress drop. S is the ratio of
 96 the strength excess over the expected stress drop, $S = \frac{\tau_y - \tau_0}{\tau_0 - \tau_d}$, where τ_y is the yield stress
 97 ($\sigma_n f_0$), τ_0 is the initial stress, and τ_d is the dynamic frictional stress ($\sigma_n f_w$). Their spa-
 98 tial distribution of the initial stress τ_0 is initially informed by a kinematic slip model (Custódio
 99 et al., 2005). They successively modify the initial stresses, τ_0 , and choose the S param-
 100 eter and the characteristic slip-weakening distance D_c by trial and error to match near-
 101 source ground motions.

102 Twardzik et al. (2014) performed a simple dynamic inversion to constrain the dy-
 103 namic parameters that governed coseismic rupture. They assumed that the slip was con-
 104 fined to two elliptical patches and inverted for the geometry of the patches, the maxi-
 105 mum S parameter within the patches, and the uniform background frictional properties
 106 of the fault plane. Barbot et al. (2012) created a long-term fully dynamic seismic cycle
 107 simulation of the Parkfield section, using a Dieterich-Ruina aging rate-and-state friction
 108 law (Ruina, 1983; Dieterich, 1992). They prescribed a heterogeneous spatial distribu-
 109 tion of the difference between the friction parameters a and b , determining velocity-strengthening
 110 (VS) and velocity-weakening (VW) behavior. All other friction parameters were kept con-

111 stant. Their model reproduced an earthquake sequence of irregular M_w 6.0 mainshocks
112 with varying propagation directions. Kostka and Gallovič (2016) modified the dynamic
113 model of Barbot et al. (2012) and showed that a stress perturbation, possibly caused by
114 the nearby 1983 Coalinga-Nuñez earthquakes, may have delayed the occurrence of the
115 2004 Parkfield mainshock.

116 1.3 Afterslip and aftershocks

117 An extended period of exceptionally large postseismic deformation followed the 2004
118 Parkfield earthquake. At the surface, the San Andreas fault zone at Parkfield consists
119 of two main fault branches, the main San Andreas fault (SAF) and the Southwest Frac-
120 ture Zone (SWFZ), which are likely connected below 6 km depth (Simpson et al., 2006).
121 During the 2004 Parkfield earthquake, the SWFZ ruptured coseismically. The SAF slipped
122 postseismically, and afterslip at the surface was detected only hours after the event (Rymer
123 et al., 2006; Langbein et al., 2006; Lienkaemper et al., 2006; Jiang et al., 2021a). Murray
124 and Langbein (2006) estimated the moment of the postseismic slip during the first 60
125 days following the earthquake to be 2×10^{18} Nm, which is larger than the coseismic mo-
126 ment release of 1.3×10^{18} Nm. Postseismic slip occurred mainly above the coseismic rup-
127 ture zone and further to the northwest (Langbein et al., 2006; Johanson et al., 2006).
128 Surface afterslip reached 20–30 cm one year after the earthquake (Lienkaemper et al.,
129 2006). Jiang et al. (2021a) combined high-rate with daily GPS solutions to study the
130 early afterslip of the 2004 Parkfield event and found that early afterslip-associated stress
131 changes appear synchronized with local aftershock rates.

132 Stress changes induced by coseismic slip and/or afterslip have been proposed to drive
133 aftershock activity (e.g., Churchill et al., 2024). The 2004 Parkfield aftershocks appear
134 mainly concentrated in two near horizontal streaks bordering the coseismic rupture zone,
135 one between 4–6 km depth and the other one between 8–10 km depth (Thurber et al.,
136 2006). Seismicity migrated along-strike and along-dip during the months after the earth-
137 quake, which has been interpreted as an indication of afterslip acting as the main driver
138 of aftershocks (Peng & Zhao, 2009; Jiang et al., 2021a). However, Cattania et al. (2015)
139 suggest that secondary triggering of aftershocks by earlier aftershocks may have played
140 a more important role, and Churchill et al. (2022)’s global statistical analysis found no
141 correlation between the relative afterslip moment and large aftershock activity.

142 **1.4 Dynamic earthquake source inversion**

143 The benefits of inverting for dynamic parameters to construct physically consis-
144 tent source models have been recognized long ago (Fukuyama & Mikumo, 1993; Peyrat
145 & Olsen, 2004; Twardzik et al., 2014), and recent advances in computational capabil-
146 ities enable inverting for multiple spatial-variable dynamic parameters. Gallovič et al.
147 (2019a) established a Bayesian dynamic source inversion framework, constraining the spa-
148 tially variable linear slip-weakening friction dynamic parameters (fault prestress, strength
149 and characteristic slip-weakening distance) across a finite, planar fault. This method has
150 been applied to the 2016 M_w 6.2 Amatrice (Gallovič et al., 2019b) and 2020 M_w 6.8 Elazığ
151 earthquake (Gallovič et al., 2020), using strong ground motion observations to constrain
152 dynamic rupture parameters and quantify their uncertainties. Premus et al. (2022) ex-
153 tended the method to rate-and-state friction, which enables jointly simulating coseismic
154 slip and afterslip in the same framework. Their dynamic source inversion of the 2014 M_w 6.0
155 South Napa California earthquake constrained by co- and postseismic strong ground mo-
156 tion and GPS data illuminated how variable prestress and frictional conditions on the
157 fault govern the spatial separation between shallow coseismic and postseismic slip, the
158 progression of afterslip driving deep off-fault aftershocks, and the coseismic slip distri-
159 bution.

160 Here, we apply the approach introduced in Premus et al. (2022) to the extensive
161 seismic and geodetic observations of the 2004 Parkfield earthquake. We are especially
162 interested in investigating the interrelation of coseismic slip and the exceptionally large
163 amount of afterslip in a uniform, data-driven modeling framework. We jointly invert this
164 data to establish an ensemble of dynamic models that simultaneously describe the co-
165 seismic and three months of postseismic slip evolution. We detail the complex coseismic
166 and postseismic faulting dynamics of a preferred joint model. We find new evidence for
167 the coseismic rupture phase involving distinctly different rupture styles and explore the
168 complex fault slip transition from the coseismic to the postseismic phase. We investi-
169 gate which dynamic parameters govern different coseismic and afterslip rupture styles
170 and analyze trade-offs between the dynamic parameters. We find different coseismic rup-
171 ture termination mechanisms imprinting on the evolution of afterslip. We jointly quan-
172 tify the average values and variability of coseismic source characteristics, including stress
173 drop, fracture energy, and radiation efficiency, as well as afterslip kinematics such as rise

174 time, propagation speed, and spatial heterogeneity and extent based on physics-based
 175 *and* data-driven models.

176 **2 Methods**

177 This section summarizes the forward and inverse modeling methods and seismic
 178 and geodetic data sets used in this study. First, we introduce the friction law that fa-
 179 cilitates the dynamic description of our problem. Then, we present the two stages of our
 180 forward model and the respective numerical solvers. Next, we describe the Bayesian in-
 181 version method, the Parallel Tempering Markov chain Monte Carlo approach. We de-
 182 tail the data used to constrain the inversion and our model parameterization. Lastly, we
 183 present our inversion strategy.

184 **2.1 Fast-velocity-weakening rate-and-state friction**

185 We use a fast-velocity-weakening rate-and-state friction law (Ampuero & Ben-Zion,
 186 2008; Noda et al., 2009) to simulate coseismic and postseismic slip in the same model-
 187 ing framework (Premus et al., 2022).

188 The following equations govern the fault’s frictional resistance (Fig. 1b, Dunham
 189 et al., 2011):

$$190 \quad \tau = \sigma_n a \operatorname{arsinh} \left[\frac{\dot{s}}{2\dot{s}_0} \exp \left(\frac{\Psi}{a} \right) \right], \quad (1)$$

$$191 \quad \frac{d\Psi}{dt} = -\frac{\dot{s}}{L} (\Psi - \Psi_{SS}), \quad (2)$$

$$192 \quad \Psi_{SS} = a \log \left[\frac{2\dot{s}_0}{\dot{s}} \sinh \left(\frac{f_{SS}}{a} \right) \right], \quad (3)$$

$$193 \quad f_{SS} = f_w + \frac{f_{LV} - f_w}{\left(1 + \left(\frac{\dot{s}}{\dot{s}_w} \right)^8 \right)^{\frac{1}{8}}}, \quad (4)$$

$$194 \quad f_{LV} = f_0 - (b - a) \log \left(\frac{\dot{s}}{\dot{s}_0} \right). \quad (5)$$

Eq. 1 gives the frictional resistance τ , which depends on the normal stress σ_n , the direct effect parameter a , the slip rate \dot{s} , the reference slip rate \dot{s}_0 , and the state variable Ψ . Eq. 1 is regularized to avoid divergence at $\dot{s} = 0$ (Rice & Ben-Zion, 1996; Lapusta et al., 2000). Eq. 2 is an ordinary differential equation describing the evolution of the state variable Ψ . L is the characteristic slip distance, and Ψ_{SS} is the steady-state value of the state variable, which is given by Eq. 3. Eq. 4 computes the steady-state friction f_{SS} , which depends on the weakened friction coefficient f_w , the slip rate \dot{s} , the weakening slip rate \dot{s}_w , and the low-velocity steady-state friction coefficient f_{LV} . At $\dot{s} > \dot{s}_w$, f_{SS} drops rapidly from f_{LV} to f_w , with the $1/\dot{s}$ behavior resembling thermal weakening processes at coseismic slip rates such as flash-heating (Rice, 2006; Beeler et al., 2008). Eq. 5 calculates the low-velocity steady-state friction f_{LV} from the steady-state friction coefficient, the slip rate \dot{s} and the reference slip rate \dot{s}_0 , and the difference between the state evolution parameter b and the direct effect parameter a , which determines if the frictional behavior is velocity-weakening ($b - a > 0$) or velocity-strengthening ($b - a < 0$). We set the reference slip rate to 10^{-6} m/s, a common choice in dynamic rupture simulations (Harris et al., 2018). We note that the initial slip rate \dot{s}_{init} is a dynamic inversion parameter (Table 1) and differs from the reference slip rate \dot{s}_0 .

2.2 Joint dynamic rupture and afterslip forward model

The forward model consists of two stages, the coseismic and the postseismic phase, implemented using a 3D fully dynamic and a 3D quasi-dynamic method, respectively (Premus et al., 2022). In the coseismic stage, we model the earthquake dynamic rupture propagation with the code FD3D-TSN (Premus et al., 2020) based on an efficient GPU implementation of a finite-difference method. The code uses a fourth-order accurate staggered-grid method with a traction-at-split node implementation (Dalguer & Day, 2007) of the frictional fault interface condition.

The postseismic phase is modeled with a 3D quasi-dynamic boundary element approach (Rice, 1993; Gallovič, 2008). We solve the quasi-dynamic problem with a fifth-order Runge-Kutta method with adaptive time stepping. Both stages share the same planar fault geometry and the same distribution of dynamic parameters but will be constrained by complementary observations. The final coseismic distributions of the shear stress, slip rate, and state variable are used as the initial values of the postseismic stage.

226 Synthetic seismograms and static displacements are calculated via precomputed Green’s
 227 functions (Okada, 1985; Cotton & Coutant, 1997).

228 3D dynamic rupture simulations are computationally expensive, and using rate-
 229 and-state friction laws increases this cost compared to linear-slip weakening friction (e.g.,
 230 Heinecke et al., 2014; Uphoff et al., 2017; Krenz et al., 2021). Monte-Carlo-based Bayesian
 231 inversion approaches require many forward models (e.g., Press, 1968). Therefore, our joint
 232 dynamic coseismic and afterslip inversion requires large computational resources. The
 233 coseismic dynamic rupture propagation stage spans the first 21 s of the forward model,
 234 after which slip rates are low enough ($< 10^{-2}$ m/s) to switch to the quasi-dynamic sim-
 235 ulation in the postseismic stage lasting for 90 days. We use a finite-difference grid spac-
 236 ing of 100 m (Fig. 1d), which sufficiently samples the critical length scale of dynamic rup-
 237 ture, the process zone at the rupture tip, with an average of 6.3 points, ensuring accu-
 238 racy (Day et al., 2005). The grid spacing of the quasi-dynamic solver is 400 m.

239 2.3 Bayesian inversion method

240 We use a Bayesian framework to formulate the inverse problem (Tarantola, 2005;
 241 Gallovič et al., 2019a), where we sample the posterior probability density function (PDF)
 242 $p(\mathbf{m}|\mathbf{d})$ to gain information on the likelihood of a set of dynamic model parameters \mathbf{m}
 243 given the observed seismic waveform and geodetic displacement data \mathbf{d} :

$$244 \quad p(\mathbf{m}|\mathbf{d}) = \frac{p(\mathbf{m})p(\mathbf{d}|\mathbf{m})}{p(\mathbf{d})}. \quad (6)$$

245 We prescribe the prior PDF $p(\mathbf{m})$ as a uniform distribution between the pre-selected
 246 dynamic parameter bounds (see Table 1). The Bayesian evidence $p(\mathbf{d})$ normalizes the
 247 posterior PDF. The PDF of the data given a model $p(\mathbf{d}|\mathbf{m})$ is based on a least-square
 248 misfit between the synthetics $\mathbf{s}_i(\mathbf{m})$ and the observed data \mathbf{d}_i :

$$249 \quad p(\mathbf{d}|\mathbf{m}) = \exp\left(-\frac{1}{2} \sum_{i=1}^N \frac{\|\mathbf{s}_i(\mathbf{m}) - \mathbf{d}_i\|^2}{\sigma_i^2}\right). \quad (7)$$

250 N is the total number of stations, and σ_i are the standard deviations, which are
 251 assumed to be uncorrelated and represent the combined uncertainty of the model and
 252 data errors.

253 We explore the model space with the Parallel Tempering Markov chain Monte Carlo
 254 (MCMC) method (Sambridge, 2013). A Markov chain consists of a sequence of models
 255 where the parameters of the next model depend only on the previous model. Model pa-
 256 rameters are randomly perturbed during each step, with the step size inferred from a log-
 257 normal distribution. The new model is checked against the parameter bounds and is ei-
 258 ther directly discarded if the bounds are violated or the algorithm runs the forward sim-
 259 ulation and calculates the misfit. Proposed models with a smaller misfit are always ac-
 260 cepted. If the new misfit is larger, the proposed model is accepted with a probability given
 261 by the Metropolis-Hastings rule (Metropolis et al., 1953). The Parallel Tempering ap-
 262 proach explores the model space using several parallel Markov Chains, each with a tem-
 263 perature parameter T assigned. These Markov chains sample a modified posterior PDF:

$$264 \quad p(\mathbf{m}|\mathbf{d}, T) = c_1 p(\mathbf{m}) \exp\left(-\frac{1}{T} \frac{1}{2} \sum_{i=1}^N \frac{\|\mathbf{s}_i(\mathbf{m}) - \mathbf{d}_i\|^2}{\sigma_i^2}\right). \quad (8)$$

265 Markov Chains with higher T have smoother PDFs, which increases the probabil-
 266 ity of accepting the next step and facilitates the escape from local minima. c_1 normal-
 267 izes the PDF.

268 The Parallel Tempering algorithm proposes a temperature swap between the chains
 269 after each iteration. The probability of each swap is based on the Metropolis-Hastings
 270 rule. Final samples of the posterior PDF are drawn from the chains where $T = 1$. Sambridge
 271 (2013) demonstrated that the Parallel Tempering method is well-suited for non-linear
 272 problems with complicated PDFs and may converge more than 10 times faster than a
 273 non-tempered MCMC approach. In our specific case, each MPI rank hosts 8 Markov Chains,
 274 two with $T = 1$, and the other six temperatures are randomly drawn from a log-uniform
 275 distribution between 1 and 100, concentrating more values close to 1.

276 2.4 Seismic and geodetic data

277 We include seismic and geodetic measurements, both on coseismic and postseismic
 278 time scales, as inversion data. To constrain the coseismic rupture dynamics, we use strong-
 279 motion observations at 30 near-fault stations (Fig. 1a). We excluded several near-fault
 280 stations due to missing origin times, strong fault zone effects apparent even at low fre-
 281 quencies, or pronounced site amplifications (Liu et al., 2006). We include only horizon-
 282 tal components due to the worse signal-to-noise ratio of vertical components and because

Table 1. Minimum and maximum values of the dynamic parameters subject to the inversion. \dot{s}_w and \dot{s}_{init} can only vary in the velocity-strengthening areas of the fault and have constant values of 0.1 m/s and 10^{-12} m/s in the velocity-weakening areas, respectively.

Label	Parameters	Minimum Value	Maximum Value
τ_0	Shear prestress	10^3 Pa	2×10^9 Pa
$b - a$	Difference between the direct effect and the state evolution parameter	-0.03	0.03
f_0	Reference friction coefficient at $\dot{s}_0 = 10^{-6}$	0.2	1.5
L	Characteristic slip distance	0.004 m	1.0 m
\dot{s}_w	Weakening slip rate	0.01 m/s	2.0 m/s
\dot{s}_{init}	Initial slip rate	10^{-13} m/s	1.21×10^{-9} m/s
h_x	Along-strike position of nucleation patch	28.0 km	32.0 km
h_z	Along-dip position of nucleation patch	6.5 km	9.0 km
r_{nuc}	Radius of the nucleation patch	225 m	450 m
σ_{nuc}	Stress increase within the nucleation patch	1%	60%

283 we do not allow for dip-slip (see Sec. 2.5). De-emphasizing vertical components is a com-
284 mon assumption, e.g., Liu et al. (2006) down-weight the vertical components by a fac-
285 tor of 10. The strong-motion data is integrated to velocities and filtered by a fourth-order
286 causal Butterworth filter between 0.16 Hz and 0.5 Hz. We choose a low-frequency limit
287 of 0.16 Hz to ensure a flat frequency response of all instruments (Custódio et al., 2005).
288 The chosen upper limit of 0.5 Hz mitigates the impact of the 3D velocity structure, in
289 particular, of the low-velocity fault zone, which may affect all near-fault stations (Li et
290 al., 1990; Lewis & Ben-Zion, 2010). We use 25 s long seismic waveforms during the con-
291 vergence phase (see Sec. 2.6). In the subsequent sampling phase, we limited the coseis-
292 mic waveforms to 15 s long waveforms. The chosen relatively short time windows of 25 s
293 or 15 s reduce contamination from seismic reverberations due to the 3D subsurface struc-
294 ture. We assume a universal data uncertainty of $\sigma = 0.05$ m/s when computing the pos-
295 terior probability density function (PDF) of the data (Eq. 7).

296 We use the preprocessed horizontal GPS data by Jiang et al. (2021a) that span both
297 coseismic and postseismic periods. Namely, we include the coseismic displacements at

298 12 GPS stations (Fig. 1a) and postseismic displacements at 11 GPS stations during the
 299 90-day postseismic period. We compare the postseismic observations with our synthe-
 300 tics at 35 logarithmically-spaced points in time to increase the weight and resolution of
 301 the early afterslip phase. We excluded the postseismic data from the GPS station CARH
 302 as it is located between the main trace of the SAF and the secondary SWFZ branch south-
 303 west of the SAF. Afterslip migrating from the SWFZ to the SAF likely led to the po-
 304 larity change of the postseismic deformation measured at CARH (Murray & Langbein,
 305 2006; Jiang et al., 2021a), an effect which our single fault model cannot capture. We com-
 306 pletely exclude the GPS station POMM from our analysis since it is located directly above
 307 the SWFZ and is likely strongly affected by small-scale complexities in fault geometry
 308 that we cannot capture in our planar fault model (Murray & Langbein, 2006; Custódio
 309 et al., 2009). We assign an individual uncertainty value to each GPS station calculated
 310 from the mean of the data uncertainty as given by Jiang et al. (2021a) during the included
 311 90-day period.

312 2.5 Model setup

313 Our dynamic rupture and afterslip forward model incorporates a single planar fault
 314 with a strike of 320.5° and dip of 87.2° based on the fault geometry of the SWFZ of Jiang
 315 et al. (2021a). The Green’s functions account for the fault dip, but the dynamic rupture
 316 and quasi-dynamic models assume a vertical fault plane similar to (Galović et al., 2019a,
 317 2019b; Premus et al., 2022). We place the hypocenter in the initial dynamic rupture model
 318 at 35.8154°N , 120.3667°W , and 7.5 km depth based on a matched filter relocated earth-
 319 quake catalog (Neves et al., 2022). We use two different 1D velocity profiles (Custódio
 320 et al., 2005) to calculate Green’s functions accounting for different materials on each side
 321 of the fault (Table S1). The coseismic model assumes an average of both 1D layered ve-
 322 locity profiles, while the postseismic model assumes a homogenous medium, with $v_s =$
 323 3600 m/s, $v_p = 5800$ m/s, and $\rho = 2700$ kg/m³. The coseismically used Green’s func-
 324 tions account for viscoelastic attenuation. We assume variable Q values based on the em-
 325 pirical relationship v_s : $Q_s = 0.1 v_s$ (in m/s) and $Q_p = 1.5 Q_s$ (Olsen et al., 2003).

326 Table 1 summarizes the six dynamic parameters ($\tau_0, b-a, f_0, L, \dot{s}_w, \dot{s}_{init}$) and four
 327 coseismic rupture nucleation parameters ($h_x, h_z, r_{nuc}, \sigma_{nuc}$) subject to Bayesian inver-
 328 sion. We fix the weakened friction coefficient f_w to a constant value of $f_w=0.3$ follow-
 329 ing Ma et al. (2008) and vary only the reference friction coefficient f_0 , and, thereby, the

330 “reference friction drop”, $f_0 - f_w$. Similarly, we fix the direct effect parameter a to a
 331 constant value of $a = 0.015$ and allow b to vary, altering the difference $b - a$. We assume
 332 pure strike-slip faulting without dip-slip components in both the modeling and inversion
 333 stages. Thus, the prestress τ_0 and s_{init} are scalars. The dynamic parameters (prestress
 334 and friction parameters) are defined on the model grid with 24 points along-strike and
 335 9 points along-dip (Fig. 1d). In between the grid points, the dynamic parameters are
 336 bilinearly interpolated on the denser FD (finite-difference) and QD (quasi-dynamic) grids.
 337 The such defined number of potentially free dynamic inversion parameters is 1300. How-
 338 ever, \dot{s}_w and \dot{s}_{init} can only vary in the velocity-strengthening areas of the fault and have
 339 constant values of 0.1 m/s and 10^{-12} m/s in the velocity-weakening areas, respectively.
 340 The constant \dot{s}_w and \dot{s}_{init} in the velocity-weakening regions simulate locked asperities.
 341 Therefore, the number of effectively free parameters is approximately 1100 and can dy-
 342 namically change throughout the inversion.

343 We use a temporary (for 1 s) overstressed nucleation patch around the hypocen-
 344 ter to initiate dynamic rupture. We invert for the radius of this nucleation patch and
 345 the associated shear stress increase. The along-strike and along-dip location of the cen-
 346 ter of the nucleation patch, the hypocenter, is also subject to the inversion (see Table
 347 1).

348 The effective normal stress linearly increases until a depth of 3.5 km (Fig. 1c) and
 349 then remains constant at 60 MPa at deeper depths (Rice, 1992; Suppe, 2014; Madden
 350 et al., 2022). Our profile is similar to the normal stress profile in a previous 2004 Park-
 351 field dynamic rupture forward model (Ma et al., 2008).

352 **2.6 Inversion strategy**

353 Dynamic source inversion is challenging due to the nonlinear, ill-posed nature of
 354 the very high-dimensional problem and the complicated non-convex shape of the mis-
 355 fit function. We aim to increase the inversion’s performance by choosing an initial model
 356 (IM) with a high probability density (close to the optimal model). We split the dynamic
 357 inversion workflow into a convergence phase and a sampling phase. The latter generates
 358 the ensemble for uncertainty quantification. During the convergence phase, we manu-
 359 ally modify model parameters, adjust weights and datasets, and restart the Markov chains
 360 to achieve faster convergence. Thus, only the sampling phase represents an undisturbed

361 MCMC inversion. The maximum likelihood model of the convergence phase serves as
 362 the starting model of the sampling phase. Only a few Markov chain links separate this
 363 starting model from our preferred model (Sec. 3.2)

364 A randomly chosen IM may not nucleate self-sustained rupture or produce a much
 365 larger moment magnitude than the target earthquake. Therefore, we construct an ini-
 366 tial dynamic rupture model based on the stress drop and final slip distribution of “Model
 367 B” of Ma et al. (2008), who use linear slip-weakening friction to model the coseismic rup-
 368 ture of the 2004 Parkfield earthquake. We choose the potential stress drop ($\tau_0 - \tau_d$) dis-
 369 tribution of our IM to resemble the final slip distribution of Ma et al. (2008). Then, we
 370 adapt our S parameter and weakening distance L to approximately reproduce their rup-
 371 ture velocity distribution using a few trial-and-error simulations. In addition, we ran-
 372 domly perturb the characteristic slip distance L and the prestress τ_0 by up to $\pm 10\%$ to
 373 include small-scale heterogeneity and rupture complexity. We note that our resulting dy-
 374 namic parameters (see Fig. S1) deviate from Ma et al. (2008), e.g., due to the different
 375 friction laws used.

376 Albeit the random perturbations, the rupture of the IM is very homogeneous (Fig.
 377 S2). The IM’s fit to the data is moderate (see Figs. S3 and S4). It yields a seismic vari-
 378 ance reduction of 0.04 and a coseismic GPS variance reduction of 0.87.

379 The first $\approx 500,000$ models generated during the convergence phase focus on the
 380 coseismic dynamic rupture phase (21 seconds) and 69 seconds of early afterslip. Then,
 381 we modify the best-fit model from this convergence ensemble to capture long-term (90-
 382 day) afterslip observations. We manually increase the initial slip rate and potential stress
 383 drop in certain velocity-strengthening areas to approximately match the afterslip dis-
 384 tribution of Jiang et al. (2021a) and the GPS-only model of Johanson et al. (2006). To
 385 suppress anomalously high afterslip at the free surface, we set the reference friction co-
 386 efficient to 1.2 and the prestress below 1 MPa at the free surface’s model grid points.

387 The convergence phase, including long-term afterslip, additionally visits $\approx 700,000$
 388 models. During the convergence phase, we adjust the weighting of the different data sets
 389 (strong-motion, coseismic GPS, and postseismic GPS) to ensure their respective misfits
 390 remain of the same order of magnitude. Similarly, we successively reduce the step size
 391 of the inversion parameter perturbations to keep the model acceptance rate above 10%
 392 (Table S2). We restart the Markov chains several times after finding a model with a sig-

393 nificantly improved misfit. This model then serves as a new starting model for all oth-
 394 erwise independent MPI ranks of the inversion algorithm (see Sec. 2.3).

395 We start the sampling phase after reaching a satisfying data misfit. In this final
 396 phase representing a true MCMC inversion, we let the chains sample the model space
 397 without manual interventions to obtain an ensemble of best-fitting models that can ex-
 398 plain the data similarly well. The final sampling phase of the inversion visits $\approx 800,000$
 399 models. The resulting best-fitting model ensemble contains 10,500 unique models. Dur-
 400 ing the sampling phase, all inversion meta-parameters are kept constant.

401 We run the inversion on a server with 8 Nvidia RTX A5000-GPUs and 32 AMD-
 402 EPYC-7313 CPU cores with a 3 GHz base frequency. We compute the coseismic stage
 403 on the GPUs and the postseismic stage on the CPUs. This hybrid approach allows us
 404 to exploit the hardware architecture efficiently using 24 MPI ranks (3 ranks per GPU).
 405 One solution of the joint forward model takes, on average, 5 minutes. Therefore, we can
 406 visit, on average, 4.8 joint forward models per minute. Overall, the inversion visited more
 407 than 2 million joint simulations. This sums up to over 300 days of runtime on our server
 408 or $>57,000$ hours on a single GPU.

409 **3 Results**

410 **3.1 Initial dynamic rupture model**

411 Our initial dynamic rupture model (IM), which is extended from the dynamic rup-
 412 ture model by Ma et al. (2008), already reveals interesting dynamic aspects of the 2004
 413 Parkfield rupture. We find that an unusually low potential stress drop and reference fric-
 414 tion drop ($f_0 - f_w$) are needed to match the large-scale rupture characteristics of the
 415 2004 Parkfield earthquake. The earthquake ruptured over an area larger than 20 km along
 416 strike while coseismic slip remained mostly below 25 cm, which is small considering its
 417 magnitude of M_w 6.0 (Breneman et al., 2019) and in agreement with previous observa-
 418 tional studies (e.g., Liu et al., 2006; Custódio et al., 2009). The IM requires a low av-
 419 erage potential stress drop to facilitate dynamic rupture across a wide area with a small
 420 average slip. In the IM, we set the potential stress drop to 3.0 MPa within the hypocen-
 421 tral area and to only 0.6 MPa elsewhere, where we expect coseismic rupture (see Fig.
 422 S5). Outside of the expected rupture area, the potential stress drop gradually decreases
 423 to -3.0 MPa.

424 A lower stress drop generally reduces rupture velocity (Andrews, 1976; Gabriel et
 425 al., 2012). However, several studies observed that the average rupture velocity of the 2004
 426 Parkfield earthquake is relatively fast at 2.5–3.5 km/s (e.g., Fletcher et al., 2006; Ma et
 427 al., 2008; Custódio et al., 2009). To achieve a dynamic rupture model that combines a
 428 low stress drop with moderate-to-high rupture velocity, we set the characteristic slip dis-
 429 tance within the coseismic rupture area to a small value of $L = 2$ cm and assume a small
 430 S parameter, the ratio of the strength excess over the expected stress drop. Since the
 431 weakened friction coefficient ($f_w = 0.3$) and the potential stress drop are prescribed in
 432 the IM, we choose a small reference friction $f_0 = 0.313$. This leads to a reference fric-
 433 tion drop of only 0.013, which is unusually low compared to common dynamic rupture
 434 simulation parameterizations (e.g., 0.4 in Harris et al., 2018). However, such a small ref-
 435 erence friction value is in line with results obtained from dynamic modeling of afterslip
 436 following the 2004 Parkfield earthquake (Chang et al., 2013).

437 **3.2 Preferred joint dynamic rupture and afterslip model**

438 Next, we present our preferred joint dynamic rupture and afterslip model (PM) in
 439 terms of coseismic and postseismic rupture characteristics, fit to the seismic and geode-
 440 tic observations, and distribution of dynamic parameters. We chose the PM, which is
 441 a joint dynamic rupture and 90-day afterslip simulation, to maximize the sum of the seis-
 442 mic and combined (coseismic + postseismic) GPS data variance reductions (VR). The
 443 PM model selected by this criterion achieves a better seismic fit compared to the max-
 444 imum likelihood model of the inversion.

445 *3.2.1 Dynamic parameters of the preferred joint dynamic rupture and* 446 *afterslip model*

447 Fig. 2 shows the six dynamic parameters of our PM, which are subject to the Bayesian
 448 inversion. We do not show parameters on those parts of the faults that we consider un-
 449 constrained by the inversion due to the fact that the sum of the co- and postseismic slip
 450 amplitudes remains too small.

451 *3.2.1.1 Potential stress drop, velocity-weakening and velocity-strengthening fric-* 452 *tion*

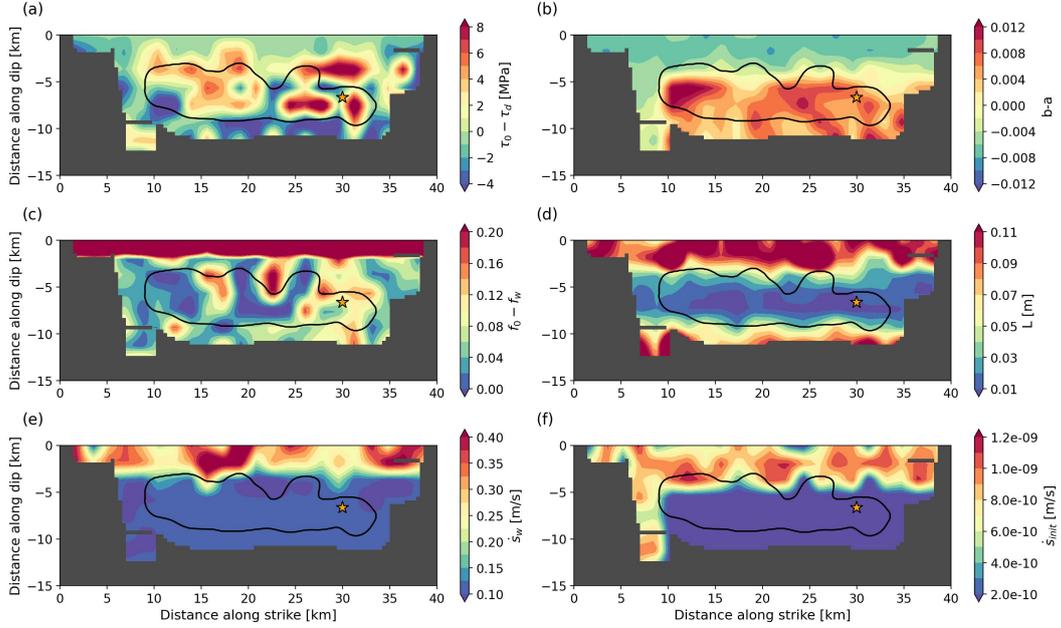


Figure 2. Dynamic parameters of the preferred joint dynamic rupture and afterslip model (PM) resulting from the Bayesian inversion. The parameters are bilinearly interpolated from the model grid (Fig. 1d) onto the grid of the quasi-dynamic solver, which has a 400 m spacing. We consider parameters to be unconstrained in all areas of the fault where the overall fault slip (coseismic + postseismic) does not exceed 10 cm within a radius of 1.2 km. We do not show dynamic parameters on these unconstrained fault grid points. The black line indicates the extent of the coseismic rupture, and the star marks the hypocenter of the mainshock. (a) Potential stress drop $\tau_0 - \tau_d$. (b) Difference between the state evolution and the direct effect parameter, $b - a$. (c) Reference friction drop $f_0 - f_w$. (d) Characteristic slip distance L . (e) Weakening slip rate \dot{s}_w . (f) Initial slip rate \dot{s}_{init} .

453 We analyze the potential stress drop, defined as $\tau_0 - \tau_d$, with the absolute prestress
 454 τ_0 and $\tau_d = f_w \sigma_n$. The spatial average of the potential stress drop within the coseis-
 455 mic rupture area is 1.0 MPa with a standard deviation of 3.4 MPa. We define the co-
 456 seismic rupture area as the region where coseismic slip exceeds 0.01 m, and the fault slip
 457 area as the region where the overall slip (coseismic + postseismic) exceeds 0.1 m within
 458 a radius of 1.2 km (visible area in Fig. 2). The fault slip area also includes well-constrained
 459 strength barriers. When considering the fault slip area, the spatial average potential stress
 460 drop reduces to 0.5 MPa, and the standard deviation to 3.0 MPa.

461 Within the coseismic rupture area, $b-a$ remains dominantly positive, which is as-
 462 sociated with VW behavior. The spatial average value is 0.0037, and the standard de-
 463 viation is 0.0048. The standard deviation being larger than its average is associated with
 464 the dynamic rupture penetrating the shallowest portion of the fault where $b-a$ is neg-
 465 ative. For the fault slip area, including regions hosting afterslip, the spatial average of
 466 $b-a$ drops to 0.000 with a standard deviation of 0.0059. The respective $b-a$ averages
 467 in the VS and VW regions are comparable to the non-constant values of Barbot et al.
 468 (2012)'s dynamic seismic cycling model, which can be approximated by $b-a = 0.004$
 469 within the coseismic rupture area and $b-a = -0.004$ within the VS regions. The range
 470 of $b-a$ within the shallow VS region agrees with the values obtained from a dynamic
 471 afterslip inversion (Chang et al., 2013).

472 *3.2.1.2 Reference friction drop and characteristic slip distance*

473 The spatial average reference friction drop within the coseismic rupture area is 0.058,
 474 and its standard deviation is 0.049. The average coseismic reference friction drop clearly
 475 increases compared to the IM (0.013) but is still small. Parts of the fault exhibit a neg-
 476 ative reference friction drop. The average reference friction drop increases considerably
 477 to 0.164 when including the afterslip regions. However, this value is strongly affected by
 478 the high reference friction coefficients at the free surface.

479 The average characteristic slip distance L within the coseismic rupture area is 0.030 m
 480 with a standard deviation of 0.024 m, corresponding to a coefficient of variation (CV;
 481 the ratio of standard deviation to average value) of $CV = 0.80$. The average and the stan-
 482 dard deviation increase to values of 0.057 m and 0.045 m, respectively, when including
 483 the afterslip regions. L noticeably increases above and beneath the top and bottom rup-
 484 ture edges, respectively.

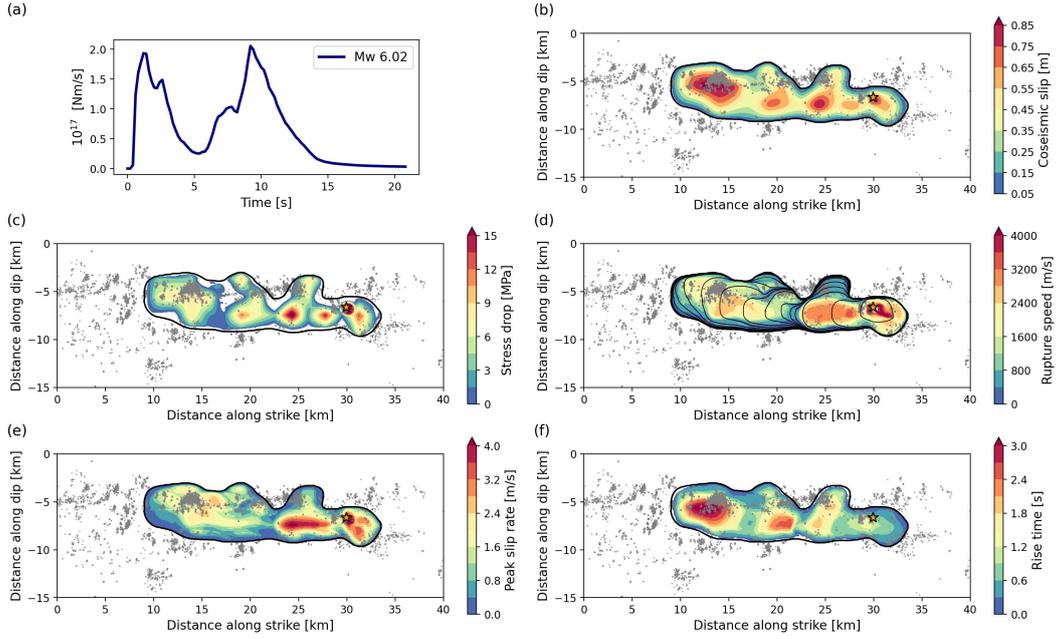


Figure 3. Coseismic dynamic rupture parameters of the PM. Grey dots show 90-day aftershock locations (Neves et al., 2022) projected on the planar fault plane, the black contour indicates the coseismic rupture extent, and the star marks the hypocenter. (a) Moment release rate and moment magnitude. (b) Coseismic slip. (c) Stress drop. (d) Local rupture speed and rupture front contours every 1 s. (e) Peak slip rate. (f) Rise time.

485 *3.2.1.3 Weakening and initial slip rates*

486 The weakening slip rate \dot{s}_w and the initial slip rate \dot{s}_{init} are allowed to vary only within
 487 VS regions (Sec. 2.5). The \dot{s}_{init} distribution shows that the shallow afterslip regions mostly
 488 creep at a slip rate of 10^{-9} m/s, which is close to the plate rate. In the shallow after-
 489 slip regions, \dot{s}_w increases to values larger than 0.2 m/s. These larger \dot{s}_w values do not
 490 directly affect the afterslip evolution because postseismic slip rates are generally smaller
 491 than \dot{s}_w .

492 *3.2.2 Coseismic rupture dynamics*

493 The spatially variable coseismic dynamic rupture characteristics of the PM are shown
 494 in Fig. 3, together with 90-day aftershock locations (Neves et al., 2022). The PM is more
 495 complex than the IM described above. In Movie S1, we provide an animation of the PM's
 496 coseismic slip rate evolution to illustrate this complexity. Coseismic rupture separates

497 into two distinct phases set apart by strong deceleration and acceleration of the rupture
 498 front. The minimum rupture speed occurs at 5 s rupture time. The PM concentrates slip
 499 within several asperities of varying sizes. The first phase of dynamic rupture propaga-
 500 tion involves several smaller asperities in the vicinity of the hypocenter. The largest as-
 501 perity is located in the northwestern part of the fault and ruptures during the second
 502 phase. In the northwest, rupture arrest is collocated with where the creeping section of
 503 the SAF is inferred to begin. Dynamic rupture is inferred to be pulse-like with high peak
 504 slip rates and low rise times during the first phase and transitions to crack-like with lower
 505 peak slip rates and high rise times within the large northwestern asperity. The transi-
 506 tion from pulse-like to crack-like rupture occurs as the rupture propagates to the north-
 507 west, towards the creeping section of the SAF.

508 *3.2.2.1 Seismic moment release and coseismic slip*

509 Fig. 3a shows the moment rate function that consists of two sharply separated peaks
 510 with a local minimum at 5 s representing the two phases of the rupture. The on-fault
 511 measured moment magnitude of M_w 6.02 corresponds to a seismic moment of $M_0 = 1.33 \times 10^{18}$ Nm,
 512 which slightly exceeds the kinematically inferred values that fall between 1.05 – 1.21×10^{18} Nm
 513 (Liu et al., 2006; Custódio et al., 2009; Twardzik et al., 2012).

514 The coseismic slip is confined to depths of 4–9 km and extends 3 km in the south-
 515 east direction and 20 km in the northwest direction from the hypocenter. The model’s
 516 average coseismic slip is 39 cm, and the highest values reach approximately 80 cm at sev-
 517 eral small asperities close to the hypocenter and within the largest asperity 14–19 km
 518 northwest of the hypocenter. Rupture extent and asperity locations agree well with pre-
 519 vious results from kinematic inversions (Custódio et al., 2009; Twardzik et al., 2012).

520 *3.2.2.2 Stress drop and rupture velocity*

521 The modeled stress drop is spatially highly variable and locally takes negative values.
 522 It reaches a local maximum of 21.5 MPa, and its average is 2.7 MPa, which is similar
 523 to Ma et al. (2008)’s dynamic rupture model but lower than the value of 4.2 MPa inferred
 524 from the lowest misfit model by Twardzik et al. (2014). The highest stress drop values
 525 are reached at the asperities close to the hypocenter. Stress drops within the large north-
 526 western asperity do not exceed 9 MPa. 7.9% of the coseismic rupture area exhibits a neg-
 527 ative stress drop.

528 The fault-local rupture velocity shown in Fig. 3d is highly variable. The average
 529 local rupture velocity of the PM is 1.4 km/s. This value is the spatial average of rup-
 530 ture speed at each grid point that coseismically slips more than 1 cm and is not equiv-
 531 alent to the average rupture velocity of 1.8 km/s measured from the hypocenter to the
 532 northern rupture extent. During the first second of dynamic rupture propagation, it reaches
 533 supershear velocity (Freund, 1979; Burridge et al., 1979; Das, 2015) of 4.0 km/s during
 534 the nucleation of the rupture, which is unexpectedly slow and below the Eshelby speed.
 535 While we do not account for a fault damage zone in our forward simulations, this result
 536 of the inversion may reflect the presence of a low-velocity fault zone in Parkfield (Bao
 537 et al., 2019). The PM ruptures with an average velocity of approximately 3.0 km/s to
 538 the northwest for the next two seconds of rupture time. After breaking through an as-
 539 perity, the rupture dramatically slows down to speeds slower than 0.8 km/s between 3
 540 and 5 seconds of simulation time. During the second phase, the rupture accelerates again
 541 to 2.5 km/s while breaking the large northwestern asperity. After 11 seconds, the rup-
 542 ture slows down until it arrests at 14 seconds after the nucleation. This slow stopping
 543 of the rupture leads to a rupture duration exceeding results from other models (Ma et
 544 al., 2008; Custódio et al., 2009; Twardzik et al., 2012).

545 *3.2.2.3 Peak slip rate and rise time*

546 The coseismic peak slip rate distribution correlates with the rupture speed distribu-
 547 tion (Schmedes et al., 2010; Gabriel et al., 2013). Slip rates reach their highest values
 548 of approximately 4.0 m/s around the hypocenter but do not exceed 2.8 m/s within the
 549 large northwestern asperity. The spatial average peak slip rate is 1.3 m/s.

550 Coseismic rise time and peak slip rate are anti-correlated and express distinctly dif-
 551 ferent rupture styles within each rupture phase. We define the coseismic rise time as the
 552 duration over which the slip rate exceeds 0.1 m/s. The rise time around the hypocen-
 553 ter is mostly below 1 s in accordance with results from kinematic studies (Liu et al., 2006;
 554 Custódio et al., 2009). Rise time is much larger in the northwestern asperity, where it
 555 exceeds 3 s.

556 *3.2.3 Seismic and geodetic verification of coseismic rupture dynamics*

557 Fig. 4 shows observed and synthetic seismic waveforms of the PM at the 30 near-
 558 field strong-motion stations used to constrain the inversion (Sec. 2.4). We show the max-

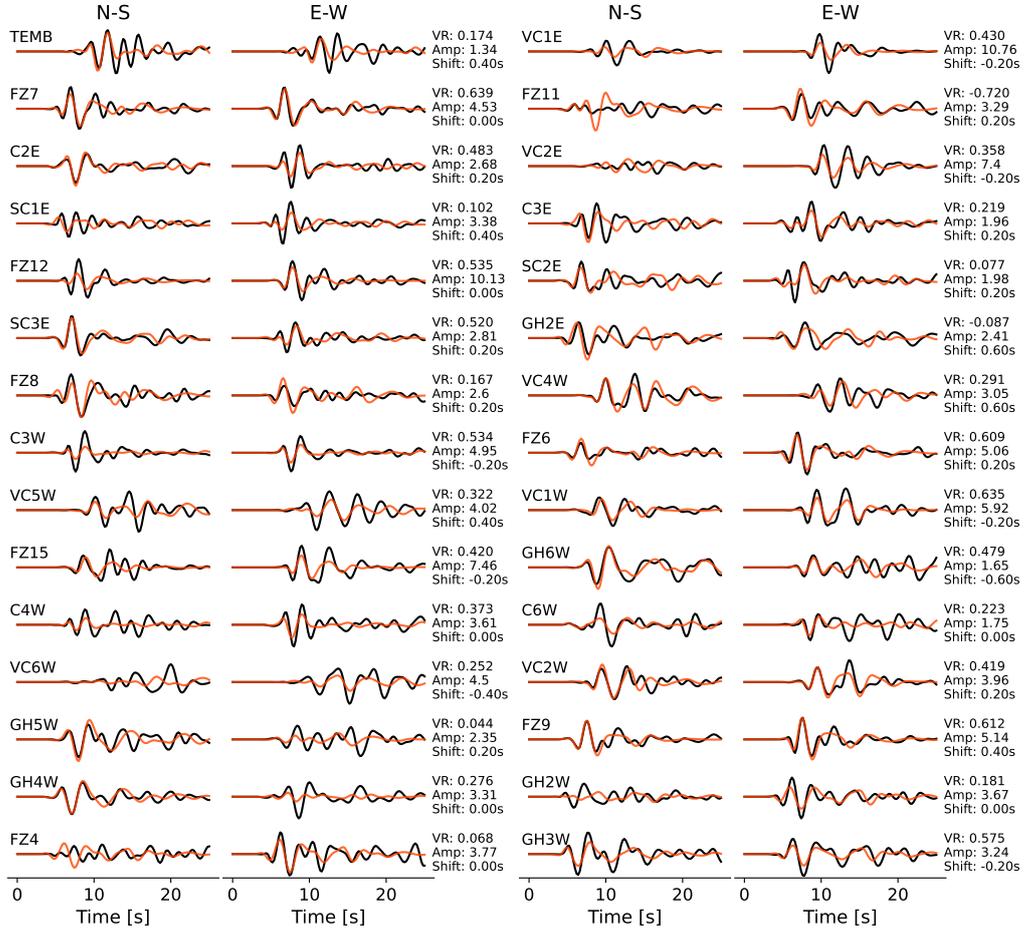


Figure 4. Observed (black, obtained through the CESMD (Center for Engineering Strong Motion Data) web service and operated by the California Strong Motion Instrumentation Program (CSMIP, California Geological Survey, 1972)) and synthetic (orange) seismic velocity waveforms from the PM, bandpass filtered between 0.16–0.5 Hz at the 30 stations used to constrain the inversion. Each waveform (synthetic and observed) is normalized by the respective station’s maximum amplitude (Amp, in cm/s, either synthetic or observed maximum). In this Figure, the observed waveforms at each station are cross-correlated and time-shifted relative to the synthetics to maximize the variance reduction (VR) and to account for unmodeled effects of topography and the 3D velocity structure.

559 inum variance reduction at each station after cross-correlation. However, during the in-
 560 version, misfits are calculated without time shifts. The overall variance reduction, cal-
 561 culated from each available seismic data point, is 0.42. We generally fit the onset of the
 562 observed seismic waveforms well. The individual stations' variance reductions vary greatly.
 563 Station FZ7 exhibits the best individual variance reduction of 0.64. Station FZ11, lo-
 564 cated nearby, has the worst fit with a strongly negative variance reduction. In general,
 565 we cannot identify a clear spatial pattern in the seismic variance reduction (see Fig. S6),
 566 except that the three stations closest to the hypocenter, where the modeled dynamic rup-
 567 ture is initiating due to overstress, have a less-than-average variance reduction between
 568 -0.09 and 0.18. This suggests that local effects may dominantly cause the misfits away
 569 from the hypocenter, e.g., site effects or the fault damage zone with highly variable char-
 570 acteristics along-strike (Lewis & Ben-Zion, 2010). We note that even kinematic source
 571 inversions using the same frequency bandwidth struggle to achieve a high seismic vari-
 572 ance reduction (Kim & Dreger, 2008).

573 Fig. 5a shows the observed and synthetic coseismic static horizontal GPS displace-
 574 ments at 12 GPS stations. Synthetic and observed coseismic displacements are compared
 575 at 90 s after the rupture onset following Jiang et al. (2021a). The overall coseismic static
 576 displacement variance reduction, calculated from each available coseismic displacement
 577 data point, is 0.95, which is better than the achieved fit of a kinematic source model con-
 578 strained by equally weighted seismic strong-motion and GPS data (see Fig. 6b in Kim
 579 & Dreger, 2008). The modeled and observed amplitudes and directions fit nearly per-
 580 fectly at most stations. Our model overpredicts the coseismic displacement at station
 581 LOWS, which is located at approximately twice the distance to the fault trace than the
 582 second farthest station.

583 *3.2.4 Geodetic verification of postseismic faulting dynamics*

584 Fig. 5b shows the normalized time evolution of the observed and modeled post-
 585 seismic horizontal displacements at 11 GPS stations that constrain the 90 days of mod-
 586 eled afterslip. Afterslip at all 11 GPS stations is largely steadily increasing, and post-
 587 seismic displacements after 90 days reach between 1–8 cm on each horizontal component.
 588 All components show similar logarithmic decay rates.

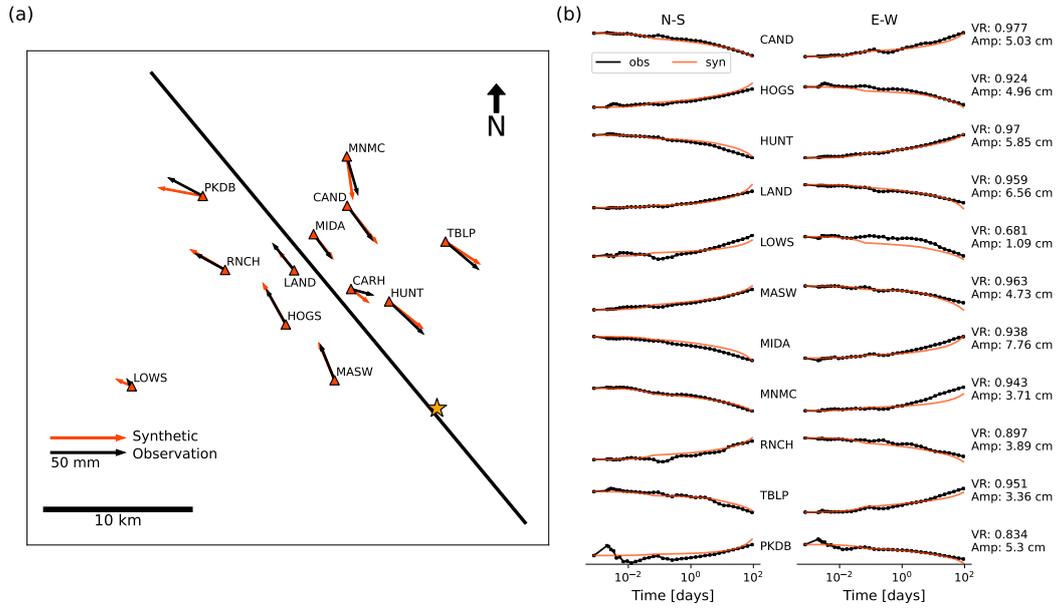


Figure 5. (a) Coseismic horizontal static displacements at 12 GPS stations. Black and orange arrows show observed (Jiang et al., 2021a) and synthetic displacements from the PM, respectively. The black line indicates the model's fault trace and the star marks the epicenter. Both synthetic and observed coseismic displacements are given at 90 s after the rupture onset. (b) Postseismic evolution of the normalized displacements at 11 GPS stations (excluding station CARH) during the first 90 days following the earthquake. Black curves show observations (Jiang et al., 2021a), and orange curves show the synthetics of the PM. The time scale is logarithmic. For each station, we annotate its variance reduction inferred after removing the coseismic displacement and its maximum amplitude.

589 The PM of our joint dynamic rupture and afterslip inversion captures the first 90
590 days of observed postseismic GPS deformation well. It achieves an overall variance re-
591 duction of 0.94 calculated from each available postseismic data point, which is remark-
592 able for a dynamically consistent joint dynamic rupture and afterslip model. We note
593 that we omit station CARH because it is affected by a polarity change due to slip mi-
594 grating to the SAF (Sec. 2.4). Similarly to the coseismic displacement misfits, station
595 LOWS has the lowest variance reduction of 0.69. However, its contribution to the over-
596 all variance reduction is small due to the small absolute displacement amplitudes at this
597 large distance to the fault. In particular, station PKDB shows spurious oscillations dur-
598 ing the first minutes and hours after the earthquake, which probably reflects observa-
599 tional artifacts from an anomalous period of the entire network (Jiang et al., 2021a). We
600 use a logarithmic time scale to accurately sample the early postseismic phase when com-
601 puting the misfits during the inversion. This leads to a lower implicit weighting of the
602 model’s last weeks. For example, we observe a late acceleration of postseismic slip evo-
603 lution at stations LAND, MASW, and PKDB 50 days after the earthquake in our model
604 but not in observations, which likely reflects this weaker penalty. The GPS stations used
605 in our inversion are expected to resolve shallow slip above the coseismic rupture area ac-
606 curately. However, their resolution is low at depths larger than 7 km and areas located
607 outside of the lateral extent of the coseismic rupture zone (Page et al., 2009).

608 Fig. 6a shows the postseismic slip distribution which our PM accumulates during
609 the modeled 90 days of afterslip. The inferred afterslip is mainly confined between the
610 free surface and the coseismic rupture area at 0–5 km depth. Postseismic slip reaches
611 maximum values of 50–60 cm within several slip patches, which is comparable to the max-
612 imum coseismic slip. Our model’s surface offsets reach 11–17 cm after 60 days, which
613 agrees well with surface offsets ranging from 12–20 cm measured on alignment arrays (Lienkaemper
614 et al., 2006). Considerable parts of the fault that slipped coseismically continue to host
615 afterslip. Afterslip can reach up to 35 cm within areas that slipped coseismically, which
616 is almost half of the maximal inferred coseismic slip. Overall, the postseismic slip evo-
617 lution reflects a smooth transition from the co- to the postseismic phase supported by
618 employing the same friction law.

619 A striking feature of the model’s afterslip distribution is a pronounced gap in the
620 afterslip located directly above the coseismic rupture area approximately 7–8 km north-
621 west of the hypocenter. Such a local lack of slip is also present in the postseismic slip

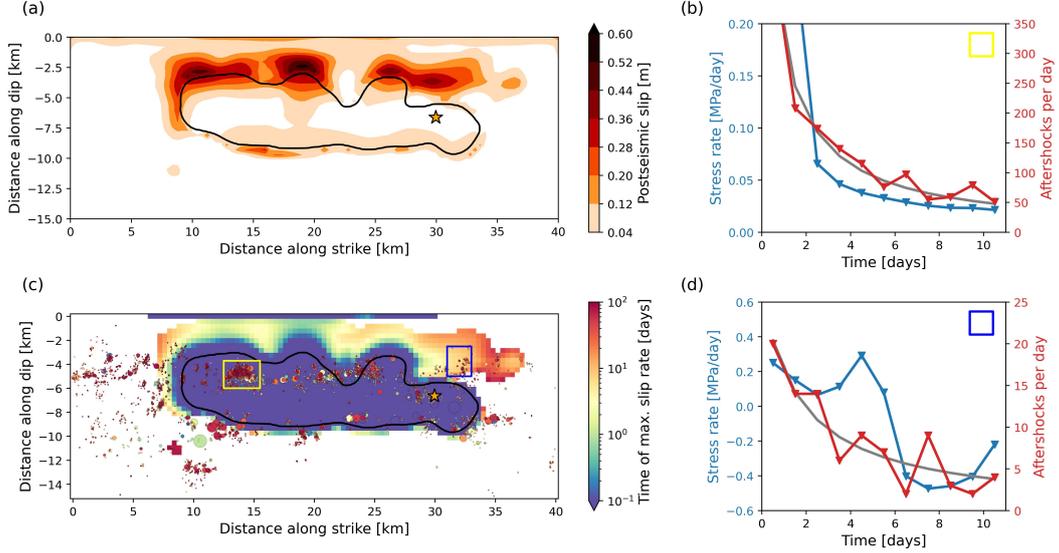


Figure 6. (a) 90-day postseismic slip of the PM. The black contour shows the extent of the coseismic rupture, and the star marks the hypocenter. (b) Aftershock rates (red) compared to average stress rates (blue) of our PM within the yellow aftershock clusters marked in (c). The grey curve shows Omori’s law ($n(t) = \frac{k}{c+t}$) fitted to the aftershock rates with $c = 0.68$ days and $k = 534.4$, where n represents the daily frequency of aftershocks depending on the time t since the mainshock. (c) Time evolution of the postseismic rupture front defined as the time of the maximum postseismic slip rate of each point where the maximum slip rate is higher than 10^{-8} m/s. The plate rate is approximately 10^{-9} m/s (Lisowski et al., 1991). Aftershock locations (Neves et al., 2022) are annotated and colored by the same logarithmic color scale, and their size is proportional to their seismic moment. The yellow and dark blue rectangles outline two aftershock clusters for which we compare aftershock rates and mean stress rates in (b) and (d). (d) Same as (b) for the aftershock cluster located within the dark blue rectangle marked in (c). Omori’s law is fitted using $c = 1.78$ days and $k = 46.51$.

622 model of Murray and Langbein (2006). In our PM, the same area that features a gap
 623 in the afterslip acts as a strong barrier to the coseismic dynamic rupture propagation
 624 and causes strong rupture deceleration starting at 3 seconds after the nucleation (Fig
 625 3b). As mentioned before, the minimum coseismic rupture speed is reached at 5 s prop-
 626 agation time.

627 ***3.2.5 Kinematics of afterslip and aftershocks***

628 Fig. 6c shows the temporal evolution of the maximum postseismic slip rate and 90-
 629 day aftershock activity following the earthquake (Neves et al., 2022). During the first
 630 three hours after the earthquake, an afterslip front develops at the shallow perimeter of
 631 the coseismic rupture and migrates up to 2 km above the coseismic slip. Surface after-
 632 slip, possibly aided by locally low confining stress in our forward models, also initiates
 633 during the first two hours after the earthquake (Langbein et al., 2005) but is initially not
 634 connected to the afterslip front migrating away from the coseismic rupture area. The fastest
 635 afterslip front is located 12 km northwest of the hypocenter and reaches the surface ap-
 636 proximately one day after the earthquake. All major afterslip patches reach their max-
 637 imum slip rate during the first 10 days following the mainshock. A small afterslip patch
 638 southeast of the hypocenter spontaneously emerges 10 days after the event and later con-
 639 nects to an afterslip front originating from the coseismic rupture area. The maximum
 640 modeled slip rate within this emerging afterslip patch reaches 10^{-6} m/s. However, the
 641 afterslip inferred at the southeastern part of the fault has a higher uncertainty as the
 642 sensitivity of the GPS network is lower (see Sec. 3.3.1 and Page et al., 2009).

643 Aftershock locations are related to the coseismic slip distribution. At the bottom
 644 and the lateral sides of the coseismic rupture area, aftershocks are mostly located at the
 645 edge or outside of the coseismic rupture area. A band of aftershocks, including the most
 646 active clusters, occurs mostly within the coseismic rupture zone between 4–6 km depth.
 647 Below 6 km depth, the coseismic rupture area is widely depleted of aftershocks reflect-
 648 ing coseismic stress release.

649 To analyze the spatiotemporal relationship between afterslip and aftershocks, we
 650 compare afterslip stressing rates and aftershock seismicity evolution with time. Figs. 6b,d
 651 show aftershock rates of two aftershock clusters during the first 10 days after the main-
 652 shock. The aftershock rate of the largest aftershock cluster (yellow rectangle) compares

653 well to our model’s mean stressing rate within the cluster region. The decay of the af-
 654 tershock rate n with time since the mainshock t follows Omori’s law ($n(t) = \frac{k}{c+t}$, grey
 655 curve in Fig. 6b) with $c = 0.68$ days. The inferred c value in this area falls within the
 656 typical range of 0–1 days and is often associated with incomplete detection of small events
 657 (Utsu et al., 1995; Kagan & Houston, 2005).

658 Aftershocks located within the blue rectangle in Fig. 6c may be driven by an af-
 659 terslip front that arrives 5–6 days after the mainshock. This afterslip front originates 4 km
 660 northwest from the hypocenter and propagates backward in the southeast direction. The
 661 average stressing rate within this region shows considerable complexity due to the pas-
 662 sage of the afterslip front. The average stress rate decreases during the first days after
 663 the mainshock. However, after 3 days, it starts to increase again, peaking at 4.5 days,
 664 which is aligned with the arrival of the afterslip stress front. Then, the stress rate rapidly
 665 decreases and turns negative due to the stress release caused by the passing afterslip. This
 666 may explain the observed considerable aftershock increase 7.5 days after the mainshock,
 667 which coincides with the maximum negative stress rate in our model. It is difficult to
 668 apply Omori’s law to this aftershock cluster. To match the aftershock rate peak at 7.5 days,
 669 an unusually large c value of 1.78 is required. Removing the peak reduces c to 1.54, which
 670 is yet larger than typical values.

671 Fig. 7a shows the afterslip rise times of the PM, which vary by more than two or-
 672 ders of magnitude. Within the coseismic rupture area, afterslip rise times are short and
 673 range between a few hours to a few days. Outside the coseismic rupture area, afterslip
 674 rise times rapidly increase to weeks and months. This increase gradually occurs over a
 675 distance of approximately 2 km away from the edge of coseismic rupture.

676 An interesting exception is a localized, approximately 4 km wide region above the
 677 hypocenter, where afterslip rise time remains constant between 15–20 days. Afterslip in
 678 this epicentral region originates from 4 km northwest along-strike from the hypocenter.
 679 There, coseismic rupture penetrates the shallow velocity-strengthening zone and initi-
 680 ates an afterslip front that propagates with constant rise time in the backward direction
 681 of coseismic rupture. This afterslip front propagates at a speed of approximately one kilo-
 682 meter per day, which is comparable to rupture velocities of slow slip events (e.g., Vavra
 683 et al., 2023). This afterslip front may drive aftershock activity (Fig. 6c and Movie S2).

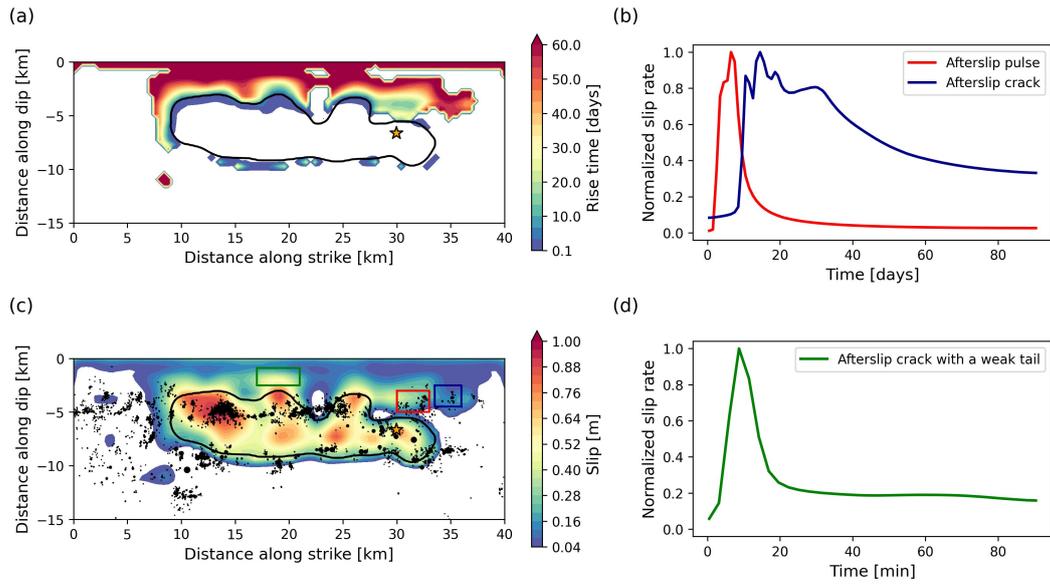


Figure 7. (a) Afterslip rise times defined as the time it takes to reach 80% of the final slip. (b) Normalized average slip rates within the red and blue rectangle marked in (c). (c) Combined coseismic slip and 90 days of postseismic slip of the PM. Colored rectangles indicate regions for which mean slip rates are shown in subplots b and d. The black line indicates the extent of the coseismic rupture, black dots show aftershock locations, and the star marks the hypocenter. (d) Normalized average slip rate within the green rectangle marked in (c).

684 The afterslip in our rate-and-state framework takes the form of different rupture
 685 styles resembling coseismic pulse-like and crack-like rupture across the same fault. The
 686 red curve in Fig. 7b shows a pulse-like afterslip slip rate function associated with the af-
 687 terslip region within the red rectangle in Fig. 7c, where the backward propagating af-
 688 terslip front is located. The average slip rate function of the adjacent region marked with
 689 a blue rectangle (blue curve in Fig. 7b) reveals a distinctly different slip rate behavior.
 690 Here, the slip rate function resembles a crack-like style of afterslip, remaining above 35%
 691 of the peak slip rate until the end of the 90-day simulation time. This region represents
 692 a coalescence of two afterslip fronts, the first arriving from the northwest region marked
 693 in red and the second originating from the spontaneously emerging afterslip patch to the
 694 southeast. However, the latter feature is associated with considerable uncertainties (see
 695 Sec. 3.3.1) and falls within the low GPS sensitivity fault region.

696 The green curve associated with the fault segment marked by a green rectangle (Fig.
 697 7c,d) shows the normalized mean slip rate function of the area with the maximum af-
 698 terslip. The time scale of the afterslip in the region marked in green (minutes) differs
 699 from the time scales of the afterslip in the regions marked in red and blue (days). The
 700 associated time scales rapidly increase with distance to the extent of the coseismic rup-
 701 ture. This slip rate function resembles an intermediate afterslip style falling in between
 702 a pulse-like and crack-like characteristic. It is characterized by a sharper peak in the be-
 703 ginning and a weaker tail remaining at approximately 20% of the peak slip rate.

704 **3.2.6 Strength excess and fracture energy**

705 Fig. 8 shows the initial strength excess ($\tau_y - \tau_0$, with $\tau_y = f_0 \sigma_n$) and the coseis-
 706 mic fracture energy distribution of our PM. The strength excess distribution implies two
 707 fundamentally different coseismic rupture-stopping mechanisms. The strength excess within
 708 the coseismic rupture area is generally low, with a spatial average of 1.05 MPa. It con-
 709 tains negative values. Shallow coseismic rupture is partly terminated at local fault strength
 710 ‘barriers’, marked with blue lines in Fig. 8a, which are areas with larger strength excess
 711 than their surroundings (Pulido & Dalguer, 2009). In distinction, coseismic rupture stops
 712 in regions with negative strength excess at three shallow locations (yellow lines in Fig.
 713 8a). We calculate the yield stress τ_y using the reference friction coefficient to approx-
 714 imate the static fault strength (see Sec. 4.4). However, the maximum friction coefficient
 715 reached during rupture is not a fixed, prescribed parameter of our forward model. In our

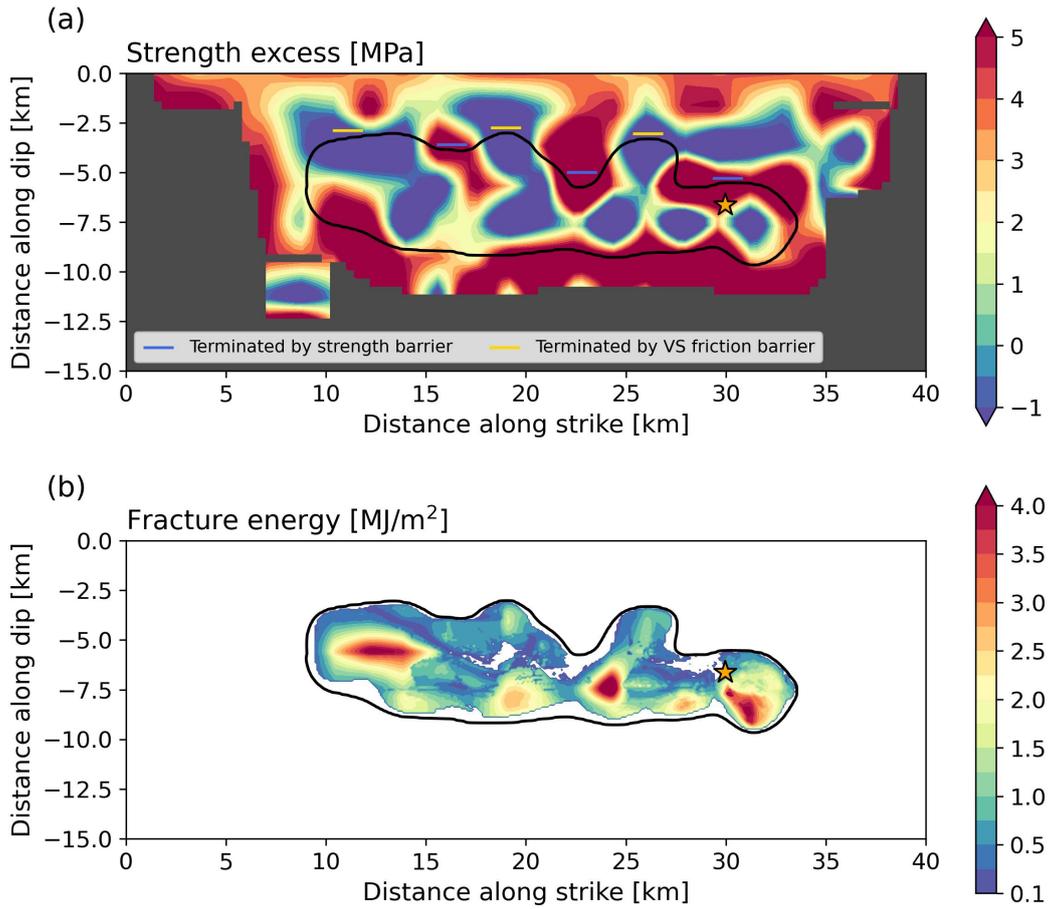


Figure 8. PM's (a) initial strength excess ($\tau_y - \tau_0$), (b) coseismic fracture energy distributions. We only show the strength excess where coseismic and postseismic slip combined exceed 10 cm somewhere within a radius of 1.2 km, which we consider as constrained by the inversion.

716 simulations, the reference friction coefficient represents a lower bound of static friction
 717 within the velocity-weakening regions (Ulrich et al., 2019).

718 We find that fracture energy is correlated with stress drop distribution (Fig. 3c).
 719 We define fracture energy per unit area as:

$$720 \quad G = \int_0^{x_{\tau_{min}}} [\tau(x) - \tau_{min}] dx, \quad (9)$$

721 where τ is shear stress, x is slip, $\tau_{min} (\approx \tau_d)$ is minimum shear stress, and $x_{\tau_{min}} (\approx$
 722 $L)$ is slip at the minimum shear stress. The three regions with the largest fracture en-
 723 ergy are located (i) southeast below the hypocenter, (ii) 7 km northwest of the hypocen-
 724 ter, where dynamic rupture decelerates abruptly, and (iii) within the large asperity 15 km
 725 northwest of the hypocenter. The spatial average of the fracture energy within the co-
 726 seismic rupture area is 0.95 MJ/m². Our inference here is similar to the 1.1 MJ/m² in-
 727 ferred for the similarly-sized 2016 M_w 6.2 Amatrice normal faulting event (Galovič et
 728 al., 2019b). A smaller value of 0.044 MJ/m² has been recently inferred from earlier 3D
 729 dynamic rupture models of a sequence of small (M_w 1.9) repeating earthquakes on the
 730 SAF 25 km northwest to the 2004 Parkfield hypocenter (Lui & Lapusta, 2018; Gabriel
 731 et al., 2023), in line with the observed fracture energy scaling with earthquake - or rup-
 732 ture - size (Cocco et al., 2023; Gabriel et al., 2023).

733 **3.3 Model ensemble characteristics and dynamic parameter trade-offs**

734 To assess model uncertainties and trade-offs, we analyze model average quantities
 735 and their variability obtained from an ensemble of best-fitting models (Sec. 2.6) contain-
 736 ing 10,500 unique model parameterizations. The ensemble average distributions of slip,
 737 rise time, afterslip, and dynamic parameters are similar to the ones of the PM. The sep-
 738 aration into two coseismic rupture phases with different rupture styles and the locations
 739 of co- and postseismic slip asperities are stable features of the model ensemble.

740 **3.3.1 Ensemble averages and uncertainties**

741 Fig. 9 shows the best model ensemble’s average and standard deviation of the co-
 742 seismic slip, the rise time, and the afterslip. The mean coseismic slip distribution is very
 743 similar to the slip distribution of the PM. Its spatial median coefficient of variation is

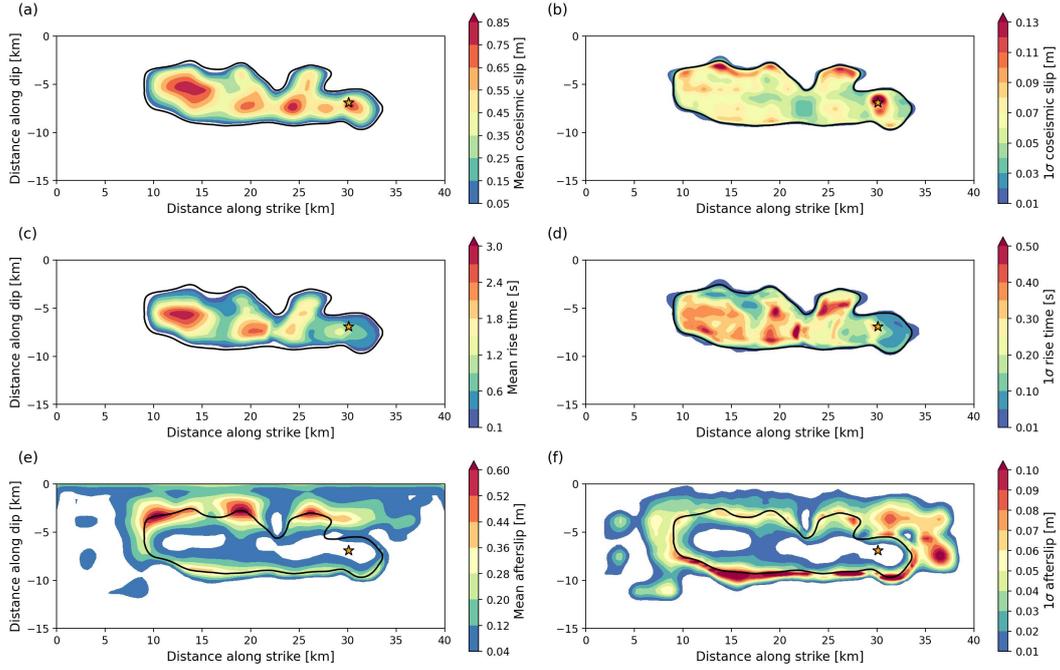


Figure 9. Ensemble average (a) coseismic slip, (c) rise time, (e) postseismic slip, and their respective standard deviations (b,d,f). Averages and standard deviations are computed from the best-fitting model ensemble containing 10,500 unique models.

744 17.3%. The standard deviation distribution has its lowest values 8 km northwest of the
 745 hypocenter, where the rupture strongly decelerates. This illustrates that this rapid rup-
 746 ture deceleration is a critical phase of the coseismic rupture dynamics. Large standard
 747 deviation values are mostly concentrated close to the rupture edges. They reach partic-
 748 ularly high values where the rupture terminates due to the transition to the velocity-strengthening
 749 regime, indicating that the abruptness of rupture termination depends on the stopping
 750 mechanism. The locally high standard deviation of the rupture contours at the same lo-
 751 cation (Fig. S7) confirms this observation.

752 The mean rise time distribution shows short rise times around the hypocenter and
 753 an area with increased rise times at the northwestern end of the rupture. The coefficient
 754 of variation of both rise-time features lies in the range of 10–20%, indicating that they
 755 are stable results of the inversion. The rise time standard deviation distribution reaches
 756 its largest value approximately 9 km northwest of the hypocenter, where the rupture ac-
 757 celerates again after nearly terminating.

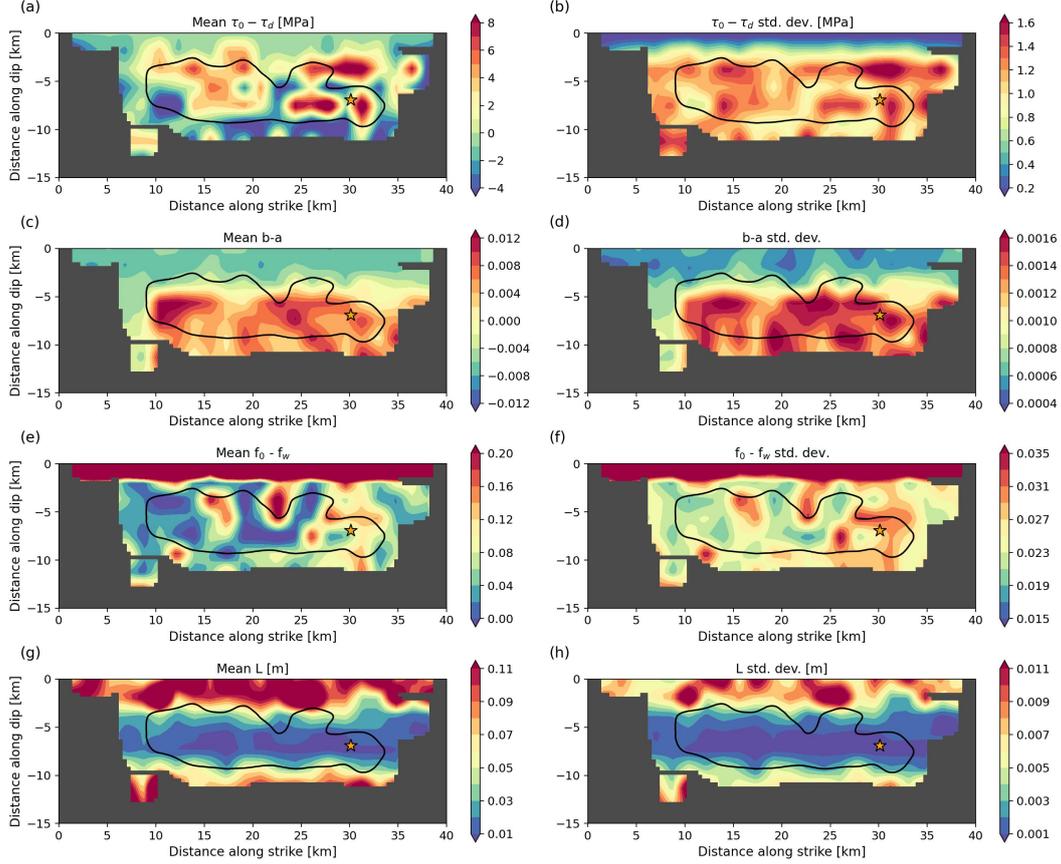


Figure 10. Mean distributions of the best-fitting model ensemble’s (a) potential stress drop $\tau_0 - \tau_d$, (c) $b - a$, (e) reference friction drop $f_0 - f_w$, (g) characteristic weakening distance L , and their respective standard deviations (b,d,f,h). The model ensemble contains 10,500 models. We mask areas where the sum of coseismic and postseismic slip does not exceed 10 cm within an area of a radius of 1.2 km, which we consider unconstrained.

758 The afterslip variability is greatest at the bottom of the coseismic rupture zone,
 759 reflecting the combined effects of varying rupture extent and the GPS network’s low res-
 760 olution. Another zone of high afterslip variability above and southeast of the hypocen-
 761 ter likely reflects the weak constraints due to the GPS network configuration, with all
 762 stations located northwest of the hypocenter. The variability is generally reduced close
 763 to the free surface, where the sensitivity of the GPS network increases.

764 The dynamic parameters do not vary extensively within the ensemble. Figure 10
 765 shows the ensemble mean and the standard deviation distributions of the potential stress
 766 drop $\tau_0 - \tau_d$, $b - a$, the reference friction drop $f_0 - f_w$, and the characteristic weakening

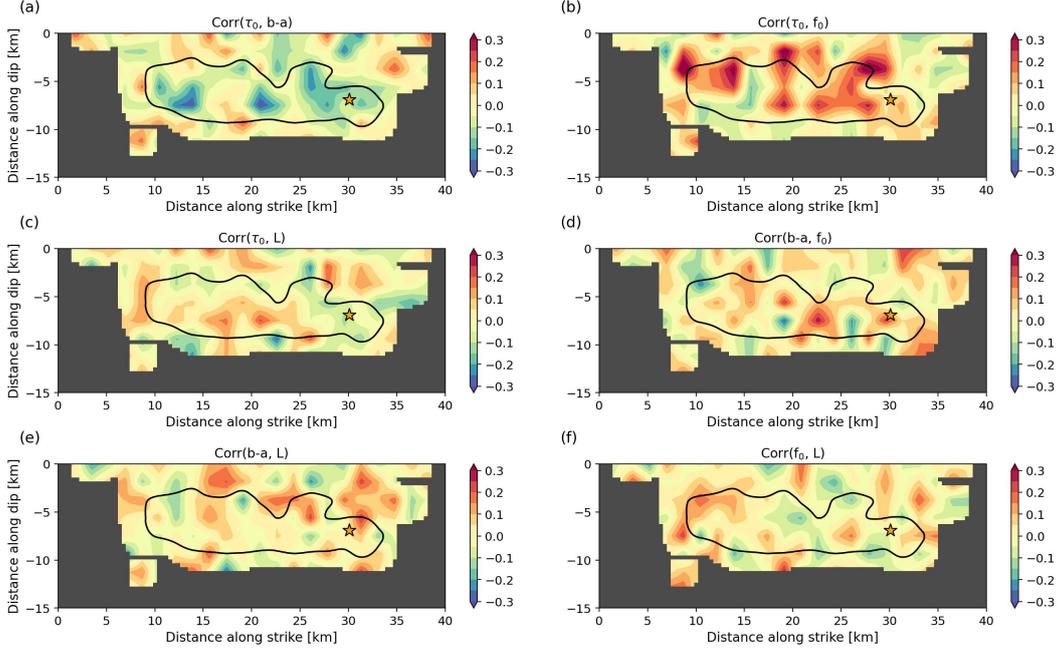


Figure 11. Ensemble correlation coefficients' spatial distribution of dynamic parameter pairs (a) τ_0 and $b - a$, (b) τ_0 and f_0 , (c) τ_0 and L , (d) $b - a$ and f_0 , (e) $b - a$ and L , (f) f_0 and L . The black contour indicates the extent of the coseismic rupture, and the star marks the hypocenter. We mask areas where the sum of coseismic and postseismic slip does not exceed 10 cm within an area of a radius of 1.2 km, which we consider unconstrained.

767 distance L . The means of all four dynamic parameters are comparable to the PM (see
 768 Fig. 2). The standard deviations are relatively small and highly correlated with the cor-
 769 responding mean distributions. Plotting the coefficient of variation of the four dynamic
 770 parameters or a strictly positive equivalent (see Fig. S8) confirms this observation. The
 771 coefficients of variation of all four parameters are spatially rather homogeneous, with val-
 772 ues ranging mostly between 4–8%. Within the coseismic rupture area, τ_0 has the small-
 773 est and L the largest relative uncertainties.

774 *3.3.2 Ensemble correlations and source parameters*

775 The prestress is locally (anti-)correlated with $b - a$ and f_0 , while overall correla-
 776 tion values between different dynamic parameters are small. Fig. 11 shows correlation
 777 coefficients of the ensemble's dynamic parameters to analyze trade-offs between them.
 778 Correlation coefficients rarely exceed ± 0.4 . Locally, prestress τ_0 and reference friction

779 coefficient f_0 share the highest positive correlation. Maximum values up to 0.4 are reached
 780 in areas where coseismic and postseismic slip overlap, likely because prestress variations
 781 can be dynamically balanced by changes in the reference friction coefficient. τ_0 and $b-$
 782 a show an anticorrelation of up to -0.3. High anticorrelation in areas with large rise times
 783 may indicate that a careful balance between τ_0 and $b-a$ is important to facilitate sus-
 784 tained crack-like rupture. Slip-weighted average correlation coefficients of the other four
 785 parameter pairs are below 0.02.

786 The dynamic source inversion approach facilitates computing fundamental earth-
 787 quake source parameters such as radiated energy and fracture energy while simultane-
 788 ously relying on observed data and the underlying physics. Fig. S9 displays histograms
 789 of various coseismic and postseismic rupture parameters of the best-fitting model ensem-
 790 ble. We find an ensemble average radiated energy of 2.19×10^{13} J and an average co-
 791 seismic fracture energy of 8.30×10^{13} J, which translates to an average radiation effi-
 792 ciency of 21%.

793 4 Discussion

794 4.1 Mixed crack- and pulse-like rupture dynamics governed by local fault 795 heterogeneity

796 It remains debated whether earthquakes predominantly propagate as cracks or as
 797 pulses (Heaton, 1990). For example, Lambert et al. (2021) hypothesize that large megath-
 798 rust events mainly rupture as ‘mild’ cracks whereas crustal strike-slip faults rupture in
 799 the form of self-healing pulses. We infer a clear transition from pulse-like (short rise time)
 800 to crack-like (long rise time) coseismic rupture of the crustal strike-slip 2004 Parkfield
 801 earthquake. This may indicate that the style of earthquake rupture rather depends on
 802 local rheological and frictional properties than on the regional tectonic setting and that
 803 one earthquake may comprise more than one rupture style (e.g., Gabriel et al., 2012).

804 We analyze the spatial correlation between rise times and dynamic parameters (Fig.
 805 S10) of our preferred model (PM) to understand the underlying factors causing the co-
 806 seismic rupture style transition. While rise time does not correlate with the potential
 807 stress drop $\tau_0 - \tau_w$, it depends on the interplay between $f_0 - f_w$, $b - a$, and L . The ref-
 808 erence friction drop exhibits the highest (anti-)correlation of -0.59 with rise time. The
 809 largest rise times are reached when the reference friction drop is smaller than 0.05. L

810 shows an anticorrelation (-0.39) with rise time and $b - a$ shows a positive correlation
 811 of 0.47 with rise time. These results imply that a velocity-weakening regime, with small
 812 L and small $f_0 - f_w$, promotes crack-like rupture. Contrary to our results, Ampuero and
 813 Rubin (2008) report an anticorrelation between $b - a$ and rise time. The overall geo-
 814 metrical simplicity of the Parkfield segment suggests that the observed rupture behav-
 815 ior is driven mainly by initial stresses and specific local frictional properties. We con-
 816 clude that it's a complex interplay of fault-local dynamic parameters that likely deter-
 817 mines the rupture style.

818 In our PM, both rupture styles produce vastly varying seismic radiation. Fig. S11
 819 shows a waveform comparison with synthetics generated by a 5 s version of our PM, in-
 820 cluding only the initial pulse-like phase. The short model's overall seismic variance re-
 821 duction reaches 95.3% of the full model's variance reduction, but the short model can-
 822 not explain the displacements measured by the GPS stations. The initial pulse-like phase
 823 produces most of the seismic radiation while accounting only for 35.7% of the seismic
 824 moment, in agreement with observations (Allmann & Shearer, 2007).

825 This is consistent with our inferred gradual transition from the coseismic to the post-
 826 seismic phase. Coseismic rupture dynamics initiate as a strongly radiating phase, fol-
 827 lowed by a mildly radiating phase, which only weakly imprints on the seismic data but
 828 produces dynamic perturbations in the GPS data (Jiang et al., 2021a). Finally, aseis-
 829 mic afterslip dominates with rise times increasing with time and distance from the co-
 830 seismic rupture area (Fig. 7). These results highlight the importance of complementary
 831 data sets to infer kinematic and dynamic source models and have important implications
 832 for seismic hazard assessment: Similarly sized earthquakes can cause vastly different ground
 833 motions based on the dominantly operating rupture style, and large earthquakes can ex-
 834 perience strong local amplifications due to dynamic rupture complexity (Schliwa & Gabriel,
 835 2023).

836 **4.2 Early supershear and rupture speed variability**

837 We observe locally pronounced rupture speed variations in our dynamic rupture
 838 inversion. While our models are based on low-frequency data, our results may explain
 839 locally observed high-frequency radiation. Similar to the rupture speed in our PM, Custódio
 840 et al. (2009) reported a supershear rupture onset with velocities above 4 km/s during

841 the first second of their kinematic source model. However, their model does not feature
 842 strong rupture deceleration after 3 seconds, although the final slip distribution is sim-
 843 ilar to our model. Fletcher et al. (2006) determined the rupture velocity of the 2004 Park-
 844 field earthquake via back-projection using a short-baseline array 12 km west of the epi-
 845 center. They also inferred a fast rupture onset but without reaching supershear speeds.
 846 In their study, the rupture starts with a velocity of 3.3 km/s and then drops to an av-
 847 erage velocity of 2.4 km/s.

848 Allmann and Shearer (2007) found a burst of high-frequency seismic radiation origi-
 849 nating at the southern edge of the northern high-slip patch approximately 13 km north-
 850 west of the hypocenter and 5.5 s after rupture initiation. Our model ensemble persis-
 851 tently features a strong rupture deceleration and subsequent acceleration between the
 852 southeastern and northwestern parts of the rupture. Such abrupt changes in rupture ve-
 853 locity cause high-frequency radiation (e.g., Madariaga, 1977; Shi & Day, 2013; Schliwa
 854 & Gabriel, 2023). The rupture speed change in our model ensemble is caused by a strong
 855 fault strength barrier (Fig. S12a) that extends from 8–3 km depth and also creates an
 856 afterslip gap (Fig. 9e). This barrier is a well-constrained feature of our model and might
 857 represent a local rheological or geometrical complexity.

858 Fletcher et al. (2006) tracked high-frequency arrivals with a short-baseline seismic
 859 array located about 12 km west of the Parkfield epicenter. They also observe strong high-
 860 frequency sources where our rupture models abruptly decelerate after the impulsive ini-
 861 tial phase. However, they do not find any high-frequency sources at the northwestern
 862 large slip patch, which is compatible with our modeled mildly radiating crack-like rup-
 863 ture.

864 **4.3 Dynamic rupture arrest**

865 We find that distinct dynamic rupture-stopping mechanisms of different parts of
 866 coseismic rupture correlate with locally distinct afterslip evolution.

867 During dynamic rupture, elastic strain energy release competes with the consump-
 868 tion of fracture energy (Ke et al., 2018; Barras et al., 2023; Cocco et al., 2023). On a pla-
 869 nar fault, dynamic rupture terminates if (i) it dynamically runs out of available strain
 870 energy; or (ii) local changes in normal stress or frictional conditions increase the required
 871 fracture energy or lead to velocity-strengthening conditions. At three shallow locations

872 (yellow lines in Fig. 8a), coseismic rupture stops in regions with negative strength ex-
 873 cess. Comparing the coseismic rupture contours with the $b - a$ distribution (Fig. 2b)
 874 reveals that dynamic rupture terminates at these locations because it enters velocity-
 875 strengthening regions. Later, these three locations form the origin of main afterslip patches
 876 (Fig. 6a). There is no or very little afterslip evolving in regions where coseismic rupture
 877 is stopped due to local strength excess barriers.

878 The dynamic parameters L and \dot{s}_w additionally contribute to the dynamic rupture
 879 arrest. When coseismic rupture propagates into velocity-strengthening parts of the fault,
 880 slip rates cannot reach the locally increased \dot{s}_w values anymore (Fig. 2e), accelerating
 881 the rupture arrest. L noticeably increases above and beneath the coseismic rupture area
 882 (Fig. 2d). However, rupture arrest in the along-strike direction is not associated with
 883 an increase of L .

884 4.4 Coseismic stress drop, friction drop and implications for the heat 885 flow paradox

886 Our modeled low average coseismic stress drop may reflect the Parkfield section's
 887 comparably short recurrence times. The PM's average on-fault measured coseismic stress
 888 drop is 2.76 MPa which is rather small. We compare the on-fault dynamic stress drop
 889 to a seismological Brune-type stress drop estimate from calculating the average stress
 890 drop from the moment rate function spectrum using the following equation (e.g., Kaneko
 891 & Shearer, 2014):

$$892 \quad \Delta\sigma_{ef} = \frac{7}{16} \left(\frac{f_c}{k\beta} \right)^3 M_0, \quad (10)$$

893 where $f_c = 0.156$ Hz is the corner frequency of a Brune spectrum (Brune, 1970)
 894 fitted to the moment rate function spectrum of the PM (Fig. 3a), $\beta = 3600$ m/s the
 895 average S-wave velocity, $M_0 = 1.33 \times 10^{18}$ Nm the seismic moment, and k is a con-
 896 stant depending on the assumed source model. The resulting $\Delta\sigma_{ef} = 2.72$ MPa repro-
 897 duces the average on-fault stress drop when assuming $k = 0.26$, which is the value for
 898 S-wave spectra of the cohesive-zone model by Kaneko and Shearer (2014). Allmann and
 899 Shearer (2009) found that moderate to large strike-slip earthquakes have a median stress
 900 drop of 10 MPa when assuming the Madariaga (1976) source model. We infer $\Delta\sigma_{ef} =$
 901 5.16 MPa when using $k = 0.21$ from the Madariaga source model, which is approximately

902 half of the 10 MPa median value that Allmann and Shearer (2009) inferred for moder-
 903 ate to large strike-slip earthquakes.

904 The SAF is a mature fault system that is assumed to operate under relatively low
 905 absolute stress levels based on the absence of a heat flow anomaly (e.g., Lachenbruch &
 906 Sass, 1980; Rice, 1992; Williams et al., 2004) and borehole measurements at the San An-
 907 dreas Fault Observatory at Depth (e.g., Hickman & Zoback, 2004). The absence of a heat
 908 flow anomaly above the SAF may be explained by statically strong and dynamically weak
 909 faults due to strong dynamic weakening at coseismic slip rates or by an effectively low
 910 static fault strength with respect to Byerlee’s law (Byerlee, 1978). A statically weak SAF
 911 may be caused by weak fault gouge (Lockner et al., 2011) or elevated pore fluid pressure
 912 (Rice, 1992).

913 Using a friction law with a rapid-weakening mechanism at coseismic slip rates al-
 914 lows faults to operate at low average shear stress (Noda et al., 2009; Ulrich et al., 2019).
 915 Our PM exhibits a small average reference friction drop of 0.058 within the coseismic
 916 rupture area, which would not align with the concept of statically strong and dynam-
 917 ically weak faults. However, our model parameter, the reference friction drop, is not nec-
 918 essarily representative of the effective friction drop. The low-velocity steady-state fric-
 919 tion f_{LV} depends on the initial slip rate \dot{s}_{init} , the reference slip rate \dot{s}_0 , and $b-a$ (see
 920 Eq. 5). The maximum friction coefficient reached during rupture is not a prescribed model
 921 parameter but varies along the fault and often exceeds f_0 , but rarely falls below this value.
 922 We measure $f_{max} = \tau_{max}/\sigma_0$, where τ_{max} is the maximum shear stress at a given point
 923 on the fault, to analyze the static fault strength in the preferred model and find $f_{max} =$
 924 0.66 on average within the VW regions of the coseismic rupture area, which results in
 925 an effective friction drop $f_{max} - f_w$ of on average 0.36. This larger effective friction drop
 926 is yet smaller than expected from Byerlee’s law and a lithostatic pressure gradient.

927 We note that our ensemble of dynamic rupture models might be biased by the choice
 928 of the initial model (IM), which has an even smaller average reference friction drop. Al-
 929 though we cannot exclude that an alternative dynamic rupture model with a different
 930 reference friction drop may fit the data, the construction of the IM (Sec. 3.1) demon-
 931 strates that considerably larger fracture energy is likely incompatible with the earthquake’s
 932 large-scale rupture properties. The comparably small average coseismic characteristic
 933 weakening distance of 3 cm is approximately 25% of the expected value considering the

934 earthquake’s magnitude and rupture size (Gabriel et al., 2023; Palgunadi et al., 2024).
935 As we cannot achieve a higher reference friction drop without a shorter weakening dis-
936 tance while preserving fracture energy, we consider a higher friction drop dynamic model
937 unlikely to be mechanically viable.

938 **4.5 Negative coseismic stress drop may promote afterslip and aftershocks**

939 In our PM, 7.9% of the coseismic rupture area exhibits a negative coseismic stress
940 drop. We find that the largest connected area of negative coseismic stress drop at 12–
941 13 km northwest to the hypocenter (Fig. 3c) coincides with the area of most afterslip
942 within the extent of the coseismic rupture (Fig. 6a). Mikumo and Miyatake (1995)’s dy-
943 namic rupture model of the 1984 Morgan Hill earthquake featured negative stress drops
944 to explain small slip over a shallow fault section, which they associated with velocity-
945 strengthening behavior (Quin, 1990; Blanpied et al., 1991). Similar to Mikumo and Miy-
946 atake (1995)’s model, our results include a small average strength excess, which likely
947 promotes negative stress drops. Using dynamic-weakening friction, Noda and Lapusta
948 (2010) inferred regions of negative stress drop also for velocity-weakening areas with slip
949 larger than the average slip.

950 We observe that areas of negative stress drop align with increased aftershock ac-
951 tivity. Custódio et al. (2009) found that aftershocks tend to occur in regions of negative
952 stress change in a stress change model inferred from a kinematic slip model. Here, we
953 observe an interesting relationship between the aftershock locations and the slip distri-
954 bution of our PM, which is compatible with this observation. At the bottom and the lat-
955 eral edges of the coseismic rupture area, aftershocks are mostly located outside of the
956 coseismic rupture area (Fig. 6c), where a stress increase is expected (Fig. S13). In con-
957 trast, the shallow aftershock clusters between 4–6 km depth occur still within the coseis-
958 mic rupture zone, where a static stress change model would produce a negative stress
959 change. In our rate-and-state friction model, shallow rupture is often stopped by velocity-
960 strengthening friction. The shallow aftershocks coincide with the transition from a velocity-
961 weakening to a velocity-strengthening regime (Fig. 2b). Our model demonstrates that
962 this transition zone can exhibit a considerable area of negative stress drop, which is com-
963 patible with increased aftershock activity.

964 **4.6 Limitations of this study**

965 Our 90-day afterslip simulation does not account for viscoelastic effects. Freed (2007)
 966 suggest that the 2004 Parkfield postseismic deformation was solely caused by afterslip,
 967 and viscoelastic relaxation and poroelastic rebound had no significant contribution. In
 968 distinction, Bruhat et al. (2011) argue that viscoelastic relaxation is required to explain
 969 as much as 20% of the postseismic displacement at the GPS station farthest from the
 970 source (LOWS, see Fig. 1a) 5 years after the earthquake. Based on their analysis, the
 971 contribution of viscoelastic relaxation to near-source displacements during the early post-
 972 seismic time may be negligible (see Fig. 8b in Bruhat et al., 2011).

973 Albeit running more than 2 million dynamic rupture forward simulations, our in-
 974 version visits only a tiny portion of the large model space associated with ≈ 1100 dy-
 975 namic parameters. Our inverse problem also has a large null space because wide parts
 976 of the fault do not slip significantly. By providing a reasonable IM and guiding the in-
 977 version during the convergence phase by occasionally selecting our preferred model and
 978 restarting all Markov chains with the chosen model, we were able to find an ensemble
 979 of models that explains the coseismic and postseismic data, which is a similar approach
 980 to previous studies (Galović et al., 2019b; Premus et al., 2022). However, our best-fitting
 981 model ensemble cannot be assumed to be completely independent of the initial model.
 982 While the model uncertainties that we provide represent ranges of parameters that can
 983 fit the data, we cannot expect that the uncertainty quantification is mathematically com-
 984 plete in a Bayesian probabilistic sense.

985 The overall similarity between models within the ensemble may bias the absolute
 986 correlation coefficients. We find that the correlations between the different dynamic pa-
 987 rameters of the ensemble (Fig. 11) are generally low (< 0.5). However, the correlation
 988 coefficients of the best-fitting model ensemble increase with the length of the Markov chains
 989 and might rise further when the inversion is continued.

990 The earthquake dynamic inversion problem suffers from the so-called “curse of di-
 991 mensionality” - the volume of the parameter space exponentially increases with the num-
 992 ber of parameters. Further increasing the computational resources consumed ($> 57,000$
 993 GPU hours for this study) will likely be impermissible or at least highly inefficient be-
 994 cause the error of the MCMC results decreases more slowly with the number of steps (Sokal,
 995 1997).

996 Instead, future methodological improvements may be achieved by either (i) the in-
 997 troduction of advanced methods or (ii) reducing the number of model parameters. With
 998 respect to (i), new methods such as reduced-order modeling and machine learning tech-
 999 niques may aid in considerably speeding up the forward model (Rekoske et al., 2023).
 1000 Physics-based neural networks were recently applied to the rupture problem with rate
 1001 and state friction and allow for dynamic parameter estimation as part of the training pro-
 1002 cess (Rucker & Erickson, 2023). Recently, Stiernström et al. (2024) derived an adjoint-
 1003 based inversion formulation for dynamic rupture, which may reduce the time-to-solution
 1004 of dynamic source inversions but cannot provide model uncertainties. For (ii), reducing
 1005 the number of control points by, e.g., decreasing their density at the edges of the fault
 1006 or places with no expected slip will decrease the dimensionality of the forward problem.
 1007 Similarly, using a simpler linear-slip weakening friction law requires fewer model param-
 1008 eters and computational resources but can only capture coseismic rupture dynamics (e.g.,
 1009 Gallovič et al., 2019b).

1010 5 Conclusions

1011 In this study, we conduct a joint dynamic rupture and afterslip finite-fault inver-
 1012 sion of the 2004 M_w 6.0 Parkfield earthquake, resolving the spatial variability of prestress
 1013 and fault friction parameters across time scales. Using the best-fitting model ensemble,
 1014 we delineate the uncertainty bounds of dynamic model parameters and reveal their in-
 1015 herent trade-offs. The preferred dynamic model unifies the complexities of co- and post-
 1016 seismic fault slip, jointly constrained by seismic and geodetic observations. We observe
 1017 significant spatial heterogeneity in coseismic dynamic rupture and identify a pulse-like
 1018 rupture phase followed by a crack-like rupture phase. Two distinct coseismic rupture phases
 1019 are separated by a shallow strength barrier located 7–8 km northwest of the hypocen-
 1020 ter, which nearly arrests coseismic slip and subsequently causes a pronounced gap in the
 1021 90-day afterslip evolution. Our joint rate-and-state framework elucidates distinct dynamic
 1022 rupture termination mechanisms, which are closely tied to the subsequent evolution of
 1023 afterslip. Across the entire area of fault slip, including regions hosting afterslip, the spa-
 1024 tial average of $b-a$ levels at 0.000 (with a standard deviation of 0.0059). Postseismic
 1025 slip rate functions mostly resemble crack-like behavior with rise times gradually increas-
 1026 ing with distance to the edge of the coseismic rupture area. We detect a backward prop-
 1027 agating afterslip front, which aligns with delayed aftershock activity located above the

1028 hypocenter. Our analysis provides data-constrained and physics-based estimates of source
1029 parameters and their interactions. We observe areas of negative coseismic stress drop
1030 that may explain the occurrence of shallow aftershock clusters within the coseismic rup-
1031 ture area. The inferred friction drop aligns with a statically stronger and dynamically
1032 weaker Parkfield section of the San Andreas Fault. The 10,500 best-fitting model ensem-
1033 ble’s average coseismic radiation efficiency is 0.21, its coseismic stress drop is 2.73 MPa,
1034 and its average postseismic stress drop is 0.39 MPa, despite similarly large co- and post-
1035 seismic moments. This study demonstrates how physics-based models using modern com-
1036 putational techniques can uncover new insights and unprecedented details of well-recorded
1037 earthquakes.

1038 **6 Open Research**

1039 All seismic data are obtained through the CESMD (Center for Engineering Strong
1040 Motion Data) web service and we only use stations from the California Strong Motion
1041 Instrumentation Program (CSMIP, California Geological Survey, 1972). We use processed
1042 coseismic and postseismic GPS data by Jiang et al. (2021a), which are publicly avail-
1043 able: <https://doi.org/10.5281/zenodo.4278477> (Jiang et al., 2021b). The FD3D-TSN
1044 (Premus et al., 2020) version and all required input files to run the dynamic source in-
1045 version of the 2004 Parkfield earthquake are available here: <https://doi.org/10.5281/zenodo.11072717> (Schliwa, 2024).

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1058 tute of Geophysics of LMU Munich (Oeser et al., 2006).

1059 **References**

- 1060 Allmann, B. P., & Shearer, P. M. (2007). A High-Frequency Secondary Event Dur-
 1061 ing the 2004 Parkfield Earthquake. *Science*, *318*.
- 1062 Allmann, B. P., & Shearer, P. M. (2009). Global variations of stress drop for moder-
 1063 ate to large earthquakes. *Journal of Geophysical Research: Solid Earth*, *114*.
- 1064 Ampuero, J.-P., & Ben-Zion, Y. (2008). Cracks, pulses and macroscopic asymmetry
 1065 of dynamic rupture on a bimaterial interface with velocity-weakening friction.
 1066 *Geophysical Journal International*, *173*.
- 1067 Ampuero, J.-P., & Rubin, A. M. (2008). Earthquake nucleation on rate and state
 1068 faults – Aging and slip laws. *Journal of Geophysical Research: Solid Earth*,
 1069 *113*.
- 1070 Andrews, D. J. (1976). Rupture velocity of plane strain shear cracks. *Journal of*
 1071 *Geophysical Research*, *81*.
- 1072 Bakun, W. H., Aagaard, B., Dost, B., Ellsworth, W., Hardebeck, J., Harris, R., ...
 1073 Waldhauser, F. (2005). Implications for Prediction and Hazard Assessment
 1074 from the 2004 Parkfield Earthquake. *Nature*, *437*.
- 1075 Bakun, W. H., & Lindh, A. G. (1985). The Parkfield, California, Earthquake Predic-
 1076 tion Experiment. *Science*, *229*.
- 1077 Bakun, W. H., & McEvilly, T. V. (1984). Recurrence models and Parkfield, Califor-
 1078 nia, earthquakes. *Journal of Geophysical Research: Solid Earth*, *89*.
- 1079 Bao, H., Ampuero, J. P., Meng, L., Fielding, E., Liang, C., Milliner, C., ... Huang,
 1080 H. (2019). Early and persistent supershear rupture of the 2018 magnitude 7.5
 1081 Palu earthquake. *Nature Geoscience*, *12*.
- 1082 Barbot, S., Lapusta, N., & Avouac, J.-P. (2012). Under the Hood of the Earthquake
 1083 Machine: Toward Predictive Modeling of the Seismic Cycle. *Science*, *336*.
- 1084 Barras, F., Thøgersen, K., Aharonov, E., & Renard, F. (2023). How Do Earthquakes
 1085 Stop? Insights From a Minimal Model of Frictional Rupture. *Journal of Geo-*
 1086 *physical Research: Solid Earth*, *128*.
- 1087 Beeler, N. M., Tullis, T. E., & Goldsby, D. L. (2008). Constitutive relationships
 1088 and physical basis of fault strength due to flash heating. *Journal of Geophysi-*
 1089 *cal Research: Solid Earth*, *113*.
- 1090 Bilham, R. (2005). Coseismic Strain and the Transition to Surface Afterslip
 1091 Recorded by Creepmeters near the 2004 Parkfield Epicenter. *Seismological*

- 1092 *Research Letters*, 76.
- 1093 Blanpied, M. L., Lockner, D. A., & Byerlee, J. D. (1991). Fault stability inferred
1094 from granite sliding experiments at hydrothermal conditions. *Geophysical Re-*
1095 *search Letters*, 18.
- 1096 Brengman, C. M. J., Barnhart, W. D., Mankin, E. H., & Miller, C. N. (2019).
1097 Earthquake-Scaling Relationships from Geodetically Derived Slip Distribu-
1098 tions. *Bulletin of the Seismological Society of America*, 109.
- 1099 Bruhat, L., Barbot, S., & Avouac, J.-P. (2011). Evidence for postseismic deforma-
1100 tion of the lower crust following the 2004 Mw6.0 Parkfield earthquake. *Journal*
1101 *of Geophysical Research: Solid Earth*, 116.
- 1102 Brune, J. N. (1970). Tectonic stress and the spectra of seismic shear waves from
1103 earthquakes. *Journal of Geophysical Research*, 75.
- 1104 Burridge, R., Conn, G., & Freund, L. B. (1979). The stability of a rapid mode
1105 II shear crack with finite cohesive traction. *Journal of Geophysical Research:*
1106 *Solid Earth*, 84.
- 1107 Byerlee, J. D. (1978). Friction of rocks. *Pure and Applied Geophysics*, 116.
- 1108 California Geological Survey. (1972). *California strong motion instrumentation pro-*
1109 *gram*. International Federation of Digital Seismograph Networks. doi: 10.7914/
1110 B34Q-BB70
- 1111 Cattania, C., Hainzl, S., Wang, L., Enescu, B., & Roth, F. (2015). Aftershock
1112 triggering by postseismic stresses: A study based on Coulomb rate-and-state
1113 models. *Journal of Geophysical Research: Solid Earth*, 120.
- 1114 Chang, S.-H., Avouac, J.-P., Barbot, S., & Lee, J.-C. (2013). Spatially variable fault
1115 friction derived from dynamic modeling of aseismic afterslip due to the 2004
1116 Parkfield earthquake. *Journal of Geophysical Research: Solid Earth*, 118.
- 1117 Churchill, R. M., Werner, M. J., Biggs, J., & Fagereng, Å. (2022). Relative Afterslip
1118 Moment Does Not Correlate With Aftershock Productivity: Implications for
1119 the Relationship Between Afterslip and Aftershocks. *Geophysical Research*
1120 *Letters*, 49.
- 1121 Churchill, R. M., Werner, M. J., Biggs, J., & Fagereng, r. (2024). Spatial Relation-
1122 ships Between Coseismic Slip, Aseismic Afterslip, and On-Fault Aftershock
1123 Density in Continental Earthquakes. *Journal of Geophysical Research: Solid*
1124 *Earth*, 129.

- 1125 Cocco, M., Aretusini, S., Cornelio, C., Nielsen, S. B., Spagnuolo, E., Tinti, E., &
 1126 Di Toro, G. (2023). Fracture Energy and Breakdown Work During Earth-
 1127 quakes. *Annual Review of Earth and Planetary Sciences*, 51.
- 1128 Cotton, F., & Coutant, O. (1997). Dynamic stress variations due to shear faults in a
 1129 plane-layered medium. *Geophysical Journal International*, 128.
- 1130 Custódio, S., Liu, P., & Archuleta, R. J. (2005). The 2004 Mw6.0 Parkfield, Cali-
 1131 fornia, earthquake: Inversion of near-source ground motion using multiple data
 1132 sets. *Geophysical Research Letters*, 32.
- 1133 Custódio, S., Page, M. T., & Archuleta, R. J. (2009). Constraining earthquake
 1134 source inversions with GPS data: 2. A two-step approach to combine seismic
 1135 and geodetic data sets. *Journal of Geophysical Research: Solid Earth*, 114.
- 1136 Dalguer, L. A., & Day, S. M. (2007). Staggered-grid split-node method for sponta-
 1137 neous rupture simulation. *Journal of Geophysical Research: Solid Earth*, 112.
- 1138 Das, S. (2015). Supershear Earthquake Ruptures – Theory, Methods, Laboratory
 1139 Experiments and Fault Superhighways: An Update. *Geotechnical, Geological
 1140 and Earthquake Engineering*, 39.
- 1141 Day, S. M., Dalguer, L. A., Lapusta, N., & Liu, Y. (2005). Comparison of finite
 1142 difference and boundary integral solutions to three-dimensional spontaneous
 1143 rupture. *Journal of Geophysical Research: Solid Earth*, 110.
- 1144 Dieterich, J. H. (1992). Earthquake nucleation on faults with rate-and state-
 1145 dependent strength. *Tectonophysics*, 211.
- 1146 Dunham, E. M., Belanger, D., Cong, L., & Kozdon, J. E. (2011). Earthquake Rup-
 1147 tures with Strongly Rate-Weakening Friction and Off-Fault Plasticity, Part 1:
 1148 Planar Faults. *Bulletin of the Seismological Society of America*, 101.
- 1149 Fletcher, J. B., Spudich, P., & Baker, L. M. (2006). Rupture Propagation of the
 1150 2004 Parkfield, California, Earthquake from Observations at the UPSAR. *Bul-
 1151 letin of the Seismological Society of America*, 96.
- 1152 Freed, A. M. (2007). Afterslip (and only afterslip) following the 2004 Parkfield, Cali-
 1153 fornia, earthquake. *Geophysical Research Letters*, 34.
- 1154 Freund, L. B. (1979). The mechanics of dynamic shear crack propagation. *Journal of
 1155 Geophysical Research: Solid Earth*, 84.
- 1156 Fukuyama, E., & Mikumo, T. (1993). Dynamic rupture analysis: Inversion for the
 1157 source process of the 1990 Izu-Oshima, Japan, earthquake (M = 6.5). *Journal*

- 1158 of *Geophysical Research: Solid Earth*, 98.
- 1159 Gabriel, A.-A., Ampuero, J.-P., Dalguer, L. A., & Mai, P. M. (2012). The transition
1160 of dynamic rupture styles in elastic media under velocity-weakening friction.
1161 *Journal of Geophysical Research: Solid Earth*, 117.
- 1162 Gabriel, A.-A., Ampuero, J.-P., Dalguer, L. A., & Mai, P. M. (2013). Source proper-
1163 ties of dynamic rupture pulses with off-fault plasticity. *Journal of Geophysical
1164 Research: Solid Earth*, 118.
- 1165 Gabriel, A.-A., Garagash, D. I., Palgunadi, K. H., & Mai, P. M. (2023). *Fault-
1166 size dependent fracture energy explains multi-scale seismicity and cascading
1167 earthquakes*.
- 1168 Gallovič, F., Valentová, L., Ampuero, J.-P., & Gabriel, A.-A. (2019a). Bayesian Dy-
1169 namic Finite-Fault Inversion: 1. Method and Synthetic Test. *Journal of Geo-
1170 physical Research: Solid Earth*, 124.
- 1171 Gallovič, F., Valentová, L., Ampuero, J.-P., & Gabriel, A.-A. (2019b). Bayesian
1172 Dynamic Finite-Fault Inversion: 2. Application to the 2016 Mw 6.2 Amatrice,
1173 Italy, Earthquake. *Journal of Geophysical Research: Solid Earth*, 124.
- 1174 Gallovič, F., Zahradník, J., Plicka, V., Sokos, E., Evangelidis, C., Fountoulakis, I., &
1175 Turhan, F. (2020). Complex rupture dynamics on an immature fault during
1176 the 2020 Mw 6.8 Elazığ earthquake, Turkey. *Commun. Earth Environ.*, 1.
- 1177 Gallovič, F. (2008). Heterogeneous Coulomb stress perturbation during earthquake
1178 cycles in a 3D rate-and-state fault model. *Geophysical Research Letters*, 35.
- 1179 Harris, R. A., Barall, M., Aagaard, B., Ma, S., Roten, D., Olsen, K., . . . Dalguer,
1180 L. (2018). A Suite of Exercises for Verifying Dynamic Earthquake Rupture
1181 Codes. *Seismological Research Letters*, 89.
- 1182 Heaton, T. H. (1990). Evidence for and implications of self-healing pulses of slip in
1183 earthquake rupture. *Physics of the Earth and Planetary Interiors*, 64.
- 1184 Heinecke, A., Breuer, A., Rettenberger, S., Bader, M., Gabriel, A.-A., Pelties, C.,
1185 . . . Dubey, P. (2014). Petascale High Order Dynamic Rupture Earthquake
1186 Simulations on Heterogeneous Supercomputers. In *SC '14: Proceedings of
1187 the International Conference for High Performance Computing, Networking,
1188 Storage and Analysis*.
- 1189 Hickman, S., & Zoback, M. (2004). Stress orientations and magnitudes in the
1190 SAFOD pilot hole. *Geophysical Research Letters*, 31.

- 1191 Jiang, J., Bock, Y., & Klein, E. (2021a). Coevolving early afterslip and aftershock
1192 signatures of a San Andreas fault rupture. *Science Advances*, 7.
- 1193 Jiang, J., Bock, Y., & Klein, E. (2021b). *Data and Models for 'Coevolving Early*
1194 *Afterslip and Aftershock Signatures of a San Andreas Fault Rupture'* [data set].
1195 Zenodo. doi: 10.5281/zenodo.4278477
- 1196 Johanson, I. A., Fielding, E. J., Rolandone, F., & Bürgmann, R. (2006). Coseismic
1197 and Postseismic Slip of the 2004 Parkfield Earthquake from Space-Geodetic
1198 Data. *Bulletin of the Seismological Society of America*, 96.
- 1199 Johnson, K. M., Bürgmann, R., & Larson, K. (2006). Frictional Properties on the
1200 San Andreas Fault near Parkfield, California, Inferred from Models of After-
1201 slip following the 2004 Earthquake. *Bulletin of the Seismological Society of*
1202 *America*, 96.
- 1203 Kagan, Y. Y., & Houston, H. (2005). Relation between mainshock rupture process
1204 and Omori's law for aftershock moment release rate. *Geophysical Journal In-*
1205 *ternational*, 163.
- 1206 Kaneko, Y., & Shearer, P. M. (2014). Seismic source spectra and estimated stress
1207 drop derived from cohesive-zone models of circular subshear rupture. *Geophys-*
1208 *ical Journal International*, 197.
- 1209 Ke, C.-Y., McLaskey, G. C., & Kammer, D. S. (2018). Rupture Termination in
1210 Laboratory-Generated Earthquakes. *Geophysical Research Letters*, 45.
- 1211 Kim, A., & Dreger, D. S. (2008). Rupture process of the 2004 Parkfield earthquake
1212 from near-fault seismic waveform and geodetic records. *Journal of Geophysical*
1213 *Research: Solid Earth*, 113.
- 1214 Kostka, F., & Gallovič, F. (2016). Static Coulomb stress load on a three-dimensional
1215 rate-and-state fault: Possible explanation of the anomalous delay of the 2004
1216 Parkfield earthquake. *Journal of Geophysical Research: Solid Earth*, 121.
- 1217 Krenz, L., Uphoff, C., Ulrich, T., Gabriel, A.-A., Abrahams, L. S., Dunham, E. M.,
1218 & Bader, M. (2021). 3D acoustic-elastic coupling with gravity: the dynam-
1219 ics of the 2018 Palu, Sulawesi earthquake and tsunami. In *Proceedings of the*
1220 *international conference for high performance computing, networking, storage*
1221 *and analysis*. Association for Computing Machinery.
- 1222 Lachenbruch, A. H., & Sass, J. H. (1980). Heat flow and energetics of the San An-
1223 dreas Fault Zone. *Journal of Geophysical Research: Solid Earth*, 85.

- 1224 Lambert, V., Lapusta, N., & Perry, S. (2021). Propagation of large earthquakes as
1225 self-healing pulses or mild cracks. *Nature*, *591*.
- 1226 Langbein, J., Borchardt, R., Dreger, D., Fletcher, J., Hardebeck, J. L., Hellweg, M.,
1227 ... Treiman, J. A. (2005). Preliminary Report on the 28 September 2004, M
1228 6.0 Parkfield, California Earthquake. *Seismological Research Letters*, *76*.
- 1229 Langbein, J., Murray, J. R., & Snyder, H. A. (2006). Coseismic and Initial Post-
1230 seismic Deformation from the 2004 Parkfield, California, Earthquake, Observed
1231 by Global Positioning System, Electronic Distance Meter, Creepmeters, and
1232 Borehole Strainmeters. *Bulletin of the Seismological Society of America*, *96*.
- 1233 Lapusta, N., Rice, J. R., Ben-Zion, Y., & Zheng, G. (2000). Elastodynamic analysis
1234 for slow tectonic loading with spontaneous rupture episodes on faults with
1235 rate- and state-dependent friction. *Journal of Geophysical Research: Solid*
1236 *Earth*, *105*.
- 1237 Lewis, M. A., & Ben-Zion, Y. (2010). Diversity of fault zone damage and trapping
1238 structures in the Parkfield section of the San Andreas Fault from comprehen-
1239 sive analysis of near fault seismograms. *Geophysical Journal International*,
1240 *183*.
- 1241 Li, Y.-G., Leary, P., Aki, K., & Malin, P. (1990). Seismic Trapped Modes in the
1242 Oroville and San Andreas Fault Zones. *Science*.
- 1243 Lienkaemper, J. J., Baker, B., & McFarland, F. S. (2006). Surface Slip Associ-
1244 ated with the 2004 Parkfield, California, Earthquake Measured on Alinement
1245 Arrays. *Bulletin of the Seismological Society of America*, *96*.
- 1246 Lisowski, M., Savage, J. C., & Prescott, W. H. (1991). The velocity field along the
1247 San Andreas Fault in central and southern California. *Journal of Geophysical*
1248 *Research: Solid Earth*, *96*.
- 1249 Liu, P., Custódio, S., & Archuleta, R. J. (2006). Kinematic Inversion of the 2004 M
1250 6.0 Parkfield Earthquake Including an Approximation to Site Effects. *Bulletin*
1251 *of the Seismological Society of America*, *96*.
- 1252 Lockner, D., Morrow, C., Moore, D., & Hickman, S. (2011). Low strength of deep
1253 San Andreas Fault gouge from SAFOD core. *Nature*, *472*.
- 1254 Lui, S. K. Y., & Lapusta, N. (2018). Modeling High Stress Drops, Scaling, Inter-
1255 action, and Irregularity of Repeating Earthquake Sequences Near Parkfield.
1256 *Journal of Geophysical Research: Solid Earth*, *123*.

- 1257 Ma, S., Custódio, S., Archuleta, R. J., & Liu, P. (2008). Dynamic modeling of
1258 the 2004 Mw 6.0 Parkfield, California, earthquake. *Journal of Geophysical*
1259 *Research: Solid Earth*, 113.
- 1260 Madariaga, R. (1976). Dynamics of an expanding circular fault. *Bulletin of the Seis-*
1261 *mological Society of America*, 66.
- 1262 Madariaga, R. (1977). High-frequency radiation from crack (stress drop) models of
1263 earthquake faulting. *Geophysical Journal International*, 51.
- 1264 Madden, E. H., Ulrich, T., & Gabriel, A.-A. (2022). The State of Pore Fluid Pres-
1265 sure and 3-D Megathrust Earthquake Dynamics. *Journal of Geophysical Re-*
1266 *search: Solid Earth*, 127.
- 1267 Metropolis, N., Rosenbluth, A. W., Rosenbluth, M. N., Teller, A. H., & Teller, E.
1268 (1953). Equation of State Calculations by Fast Computing Machines. *The*
1269 *Journal of Chemical Physics*, 21.
- 1270 Mikumo, T., & Miyatake, T. (1995). Heterogeneous distribution of dynamic stress
1271 drop and relative fault strength recovered from the results of waveform inver-
1272 sion: the 1984 Morgan Hill, California, earthquake. *Bulletin of the Seismologi-*
1273 *cal Society of America*, 85.
- 1274 Murray, J., & Langbein, J. (2006). Slip on the San Andreas Fault at Parkfield, Cal-
1275 ifornia, over Two Earthquake Cycles, and the Implications for Seismic Hazard.
1276 *Bulletin of the Seismological Society of America*, 96.
- 1277 Neves, M., Peng, Z., & Lin, G. (2022). A High-Resolution Earthquake Catalog
1278 for the 2004 Mw 6 Parkfield Earthquake Sequence Using a Matched Filter
1279 Technique. *Seismological Research Letters*, 94.
- 1280 Noda, H., Dunham, E. M., & Rice, J. R. (2009). Earthquake ruptures with thermal
1281 weakening and the operation of major faults at low overall stress levels. *Jour-*
1282 *nal of Geophysical Research: Solid Earth*, 114.
- 1283 Noda, H., & Lapusta, N. (2010). 3D simulations of long-term fault slip with dy-
1284 namic weakening: relation between locked patches and earthquake-induced
1285 stress changes. In *Workshop on earthquake source dynamics: Data and data-*
1286 *constrained numerical modeling*.
- 1287 Oeser, J., Bunge, H.-P., & Mohr, M. (2006). Cluster design in the earth sciences
1288 tethys. In M. Gerndt & D. Kranzlmüller (Eds.), *High performance computing*
1289 *and communications*. Springer Berlin Heidelberg.

- 1290 Okada, Y. (1985). Surface deformation due to shear and tensile faults in a half-
1291 space. *Bulletin of the Seismological Society of America*, 75.
- 1292 Olsen, K. B., Day, S. M., & Bradley, C. R. (2003). Estimation of Q for Long-Period
1293 (>2 sec) Waves in the Los Angeles Basin. *Bulletin of the Seismological Society*
1294 *of America*, 93.
- 1295 Page, M. T., Custódio, S., Archuleta, R. J., & Carlson, J. M. (2009). Constraining
1296 earthquake source inversions with GPS data: 1. Resolution-based removal of
1297 artifacts. *Journal of Geophysical Research: Solid Earth*, 114.
- 1298 Palgunadi, K. H., Gabriel, A.-A., Garagash, D. I., Ulrich, T., & Mai, P. M. (2024).
1299 Rupture Dynamics of Cascading Earthquakes in a Multiscale Fracture Net-
1300 work. *Journal of Geophysical Research: Solid Earth*, 129.
- 1301 Peng, Z., & Zhao, P. (2009). Migration of early aftershocks following the 2004 Park-
1302 field earthquake. *Nature Geoscience*, 2.
- 1303 Peyrat, S., & Olsen, K. B. (2004). Nonlinear dynamic rupture inversion of the 2000
1304 Western Tottori, Japan, earthquake. *Geophysical Research Letters*, 31.
- 1305 Premus, J., Gallovič, F., & Ampuero, J.-P. (2022). Bridging time scales of faulting:
1306 From coseismic to postseismic slip of the M_w 6.0 2014 South Napa, California
1307 earthquake. *Science Advances*, 8.
- 1308 Premus, J., Gallovič, F., Hanyk, L., & Gabriel, A. (2020). FD3D-TSN: A Fast and
1309 Simple Code for Dynamic Rupture Simulations with GPU Acceleration. *Seis-
1310 mological Research Letters*, 91.
- 1311 Press, F. (1968). Earth models obtained by Monte Carlo Inversion. *Journal of Geo-
1312 physical Research (1896-1977)*, 73.
- 1313 Pulido, N., & Dalguer, L. A. (2009). Estimation of the High-Frequency Radiation
1314 of the 2000 Tottori (Japan) Earthquake Based on a Dynamic Model of Fault
1315 Rupture: Application to the Strong Ground Motion Simulation. *Bulletin of the
1316 Seismological Society of America*, 99.
- 1317 Quin, H. (1990). Dynamic stress drop and rupture dynamics of the October 15, 1979
1318 Imperial Valley, California, earthquake. *Tectonophysics*, 175.
- 1319 Rekoske, J. M., Gabriel, A.-A., & May, D. A. (2023). Instantaneous Physics-Based
1320 Ground Motion Maps Using Reduced-Order Modeling. *Journal of Geophysical
1321 Research: Solid Earth*, 128.
- 1322 Rice, J. R. (1992). Fault Stress States, Pore Pressure Distributions, and the Weak-

- 1323 ness of the San Andreas Fault. In B. Evans & T. fong Wong (Eds.), *Fault*
1324 *mechanics and transport properties of rocks* (Vol. 51, p. 475-503). Academic
1325 Press.
- 1326 Rice, J. R. (1993). Spatio-temporal complexity of slip on a fault. *Journal of Geo-*
1327 *physical Research: Solid Earth*, 98.
- 1328 Rice, J. R. (2006). Heating and weakening of faults during earthquake slip. *Journal*
1329 *of Geophysical Research: Solid Earth*, 111.
- 1330 Rice, J. R., & Ben-Zion, Y. (1996). Slip complexity in earthquake fault models. *Pro-*
1331 *ceedings of the National Academy of Sciences*, 93.
- 1332 Rucker, C., & Erickson, B. A. (2023). *Physics-Informed Deep Learning of Rate-and-*
1333 *State Fault Friction*.
- 1334 Ruina, A. (1983). Slip instability and state variable friction laws. *Journal of Geo-*
1335 *physical Research: Solid Earth*, 88.
- 1336 Rymer, M. J., Tinsley, I., John C., Treiman, J. A., Arrowsmith, J. R., Clahan,
1337 K. B., Rosinski, A. M., . . . Bawden, G. W. (2006). Surface Fault Slip As-
1338 sociated with the 2004 Parkfield, California, Earthquake. *Bulletin of the*
1339 *Seismological Society of America*, 96.
- 1340 Sambridge, M. (2013). A Parallel Tempering algorithm for probabilistic sampling
1341 and multimodal optimization. *Geophysical Journal International*, 196.
- 1342 Schliwa, N. (2024). *FD3D-TSN/2004Parkfield* [software]. Zenodo. doi: 10.5281/
1343 zenodo.11072717
- 1344 Schliwa, N., & Gabriel, A. (2023). Equivalent Near-Field Corner Frequency Analysis
1345 of 3D Dynamic Rupture Simulations Reveals Dynamic Source Effects. *Seismo-*
1346 *logical Research Letters*.
- 1347 Schmedes, J., Archuleta, R. J., & Lavallée, D. (2010). Correlation of earthquake
1348 source parameters inferred from dynamic rupture simulations. *Journal of Geo-*
1349 *physical Research: Solid Earth*, 115.
- 1350 Shi, Z., & Day, S. M. (2013). Rupture dynamics and ground motion from 3-D rough-
1351 fault simulations. *Journal of Geophysical Research: Solid Earth*, 118.
- 1352 Simpson, R. W., Barall, M., Langbein, J., Murray, J. R., & Rymer, M. J. (2006).
1353 San Andreas Fault Geometry in the Parkfield, California, Region. *Bulletin of*
1354 *the Seismological Society of America*, 96.
- 1355 Sokal, A. (1997). Monte carlo methods in statistical mechanics: Foundations and

- 1356 new algorithms. In *Functional integration: Basics and applications*. Springer
 1357 US.
- 1358 Stiernström, V., Almquist, M., & Dunham, E. M. (2024). *Adjoint-based inversion*
 1359 *for stress and frictional parameters in earthquake modeling*.
- 1360 Suppe, J. (2014). Fluid overpressures and strength of the sedimentary upper crust.
 1361 *Journal of Structural Geology*, 69.
- 1362 Tarantola, A. (2005). *Inverse Problem Theory and Methods for Model Parameter Es-*
 1363 *timation*. SIAM.
- 1364 Taufiqurrahman, T., Gabriel, A.-A., Li, D., Ulrich, T., Li, B., Carena, S., ...
 1365 Gallovič, F. (2023). Dynamics, interactions and delays of the 2019 Ridge-
 1366 crest rupture sequence. *Nature*.
- 1367 Thurber, C., Zhang, H., Waldhauser, F., Hardebeck, J., Michael, A., & Eberhart-
 1368 Phillips, D. (2006). Three-Dimensional Compressional Wavespeed Model,
 1369 Earthquake Relocations, and Focal Mechanisms for the Parkfield, California,
 1370 Region. *Bulletin of the Seismological Society of America*, 96.
- 1371 Tinti, E., Casarotti, E., Ulrich, T., Taufiqurrahman, T., Li, D., & Gabriel, A.-A.
 1372 (2021). Constraining families of dynamic models using geological, geodetic
 1373 and strong ground motion data: The Mw 6.5, October 30th, 2016, Norcia
 1374 earthquake, Italy. *Earth and Planetary Science Letters*, 576.
- 1375 Titus, S. J., DeMets, C., & Tikoff, B. (2005). New slip rate estimates for the creep-
 1376 ing segment of the San Andreas fault, California. *Geology*, 33.
- 1377 Tong, X., Sandwell, D. T., & Smith-Konter, B. (2013). High-resolution interseis-
 1378 mic velocity data along the San Andreas Fault from GPS and InSAR. *Journal*
 1379 *of Geophysical Research: Solid Earth*, 118.
- 1380 Twardzik, C., Das, S., & Madariaga, R. (2014). Inversion for the physical param-
 1381 eters that control the source dynamics of the 2004 Parkfield earthquake. *Jour-*
 1382 *nal of Geophysical Research: Solid Earth*, 119.
- 1383 Twardzik, C., Madariaga, R., Das, S., & Custódio, S. (2012). Robust features of
 1384 the source process for the 2004 Parkfield, California, earthquake from strong-
 1385 motion seismograms. *Geophysical Journal International*, 191.
- 1386 Ulrich, T., Gabriel, A.-A., Ampuero, J.-P., & Xu, W. (2019). Dynamic viability of
 1387 the 2016 Mw 7.8 Kaikōura earthquake cascade on weak crustal faults. *Nature*
 1388 *Communications*.

- 1389 Uphoff, C., Rettenberger, S., Bader, M., Madden, E. H., Ulrich, T., Wollherr, S., &
1390 Gabriel, A.-A. (2017). Extreme scale multi-physics simulations of the tsunami-
1391 genic 2004 sumatra megathrust earthquake. In *Proceedings of the international*
1392 *conference for high performance computing, networking, storage and analysis*.
1393 Association for Computing Machinery.
- 1394 Utsu, T., Ogata, Y., S, R., & Matsu'ura. (1995). The Centenary of the Omori For-
1395 mula for a Decay Law of Aftershock Activity. *Journal of Physics of the Earth*,
1396 *43*.
- 1397 Vavra, E., Fialko, Y., Rockwell, T. K., Bilham, R., Stepancikova, P., Stemberk, J.,
1398 ... Stemberk, J. (2023). Characteristic Slow-Slip Events on the Superstition
1399 Hills Fault, Southern California. *ESS Open Archive*.
- 1400 Wen, Y., Cai, J., He, K., & Xu, C. (2024). Dynamic Rupture of the 2021 MW
1401 7.4 Maduo Earthquake: An Intra-Block Event Controlled by Fault Geometry.
1402 *Journal of Geophysical Research: Solid Earth*, *129*.
- 1403 Williams, C. F., Grubb, F. V., & Galanis Jr., S. P. (2004). Heat flow in the SAFOD
1404 pilot hole and implications for the strength of the San Andreas Fault. *Geo-*
1405 *physical Research Letters*, *31*.

Supporting Information for ”The linked complexity of coseismic and postseismic faulting revealed by seismo-geodetic dynamic inversion of the 2004 Parkfield earthquake”

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Additional Supporting Information (Files uploaded separately)

1. Captions for Movies S1 to S2

Introduction This document contains supplementary figures, tables, and movie captions to augment the main manuscript.

Movie S1. Coseismic slip rate evolution of the preferred dynamic rupture and afterslip model. The black contour shows the coseismic rupture extent and the star marks the hypocenter.

Movie S2. 90-day postseismic slip rate evolution of the preferred joint dynamic rupture and afterslip model. Light blue dots show aftershocks during the latest 20% of the time since the mainshock and grey dots show the remaining aftershocks since the mainshock. The black line shows the coseismic rupture extent and the star marks the hypocenter.

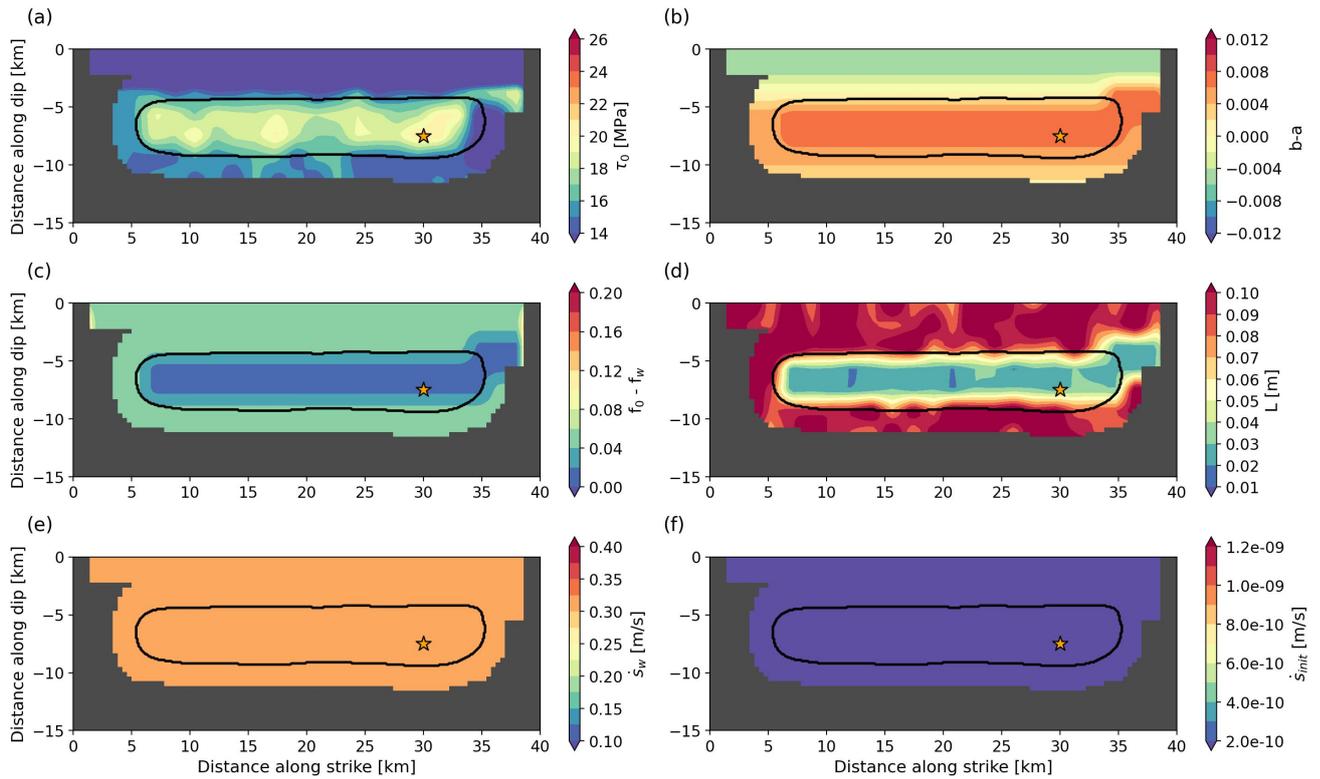


Figure S1. Dynamic parameters of the initial dynamic rupture model based on "Model B" of Ma et al. (2008). The parameters are bilinearly interpolated from the model grid (Fig. 1d) onto the grid of the quasi-dynamic solver, which has a 400 m spacing. We consider parameters to be unconstrained in all areas of the fault where the overall fault slip (coseismic + postseismic) does not exceed 10 cm within a radius of 1.2 km. We do not show dynamic parameters on these unconstrained fault grid points. The black line indicates the extent of the coseismic rupture, and the star marks the hypocenter of the mainshock. (a) Prestress τ_0 . (b) Difference between the state evolution and the direct effect parameter, $b-a$. (c) Friction drop $f_0 - f_w$. (d) Characteristic slip distance L . (e) Weakening slip rate \dot{s}_w . (f) Initial slip rate \dot{s}_{init} .

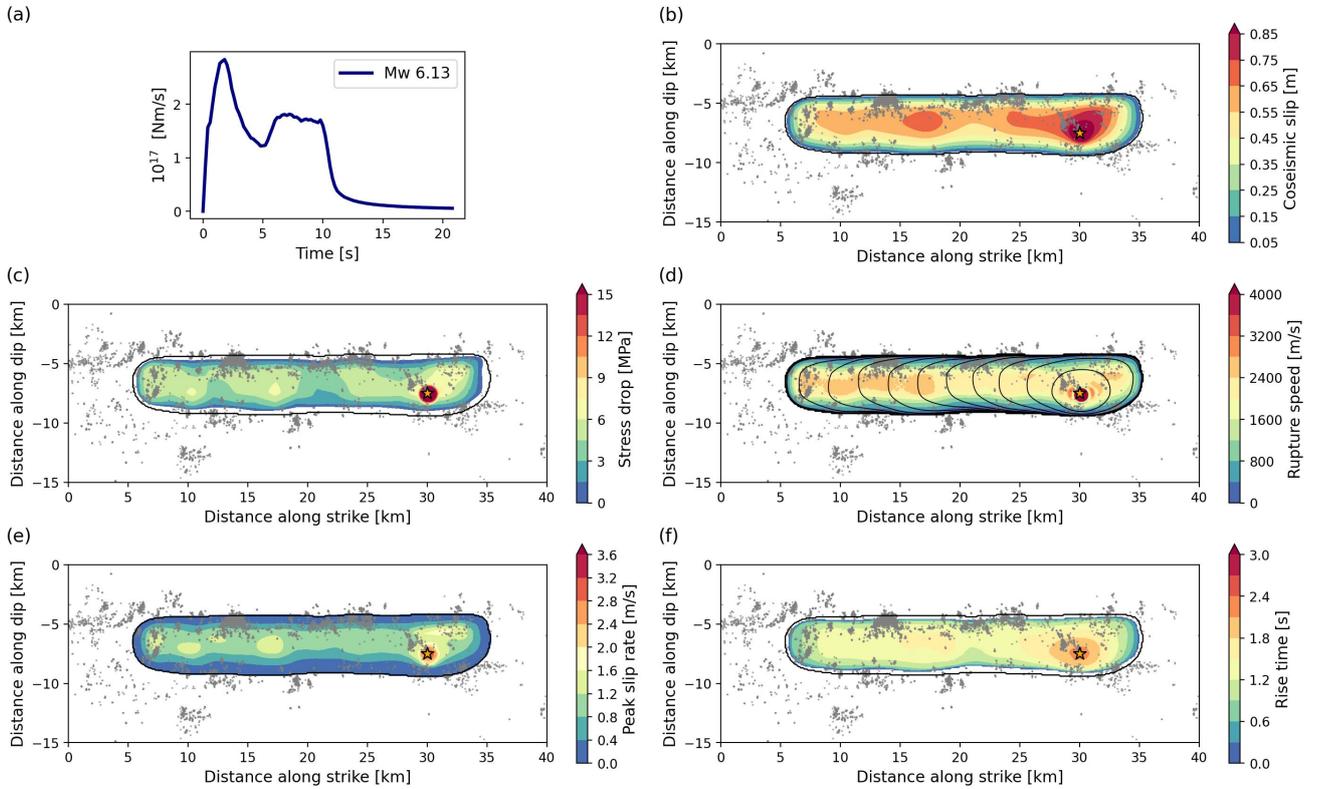


Figure S2. Coseismic dynamic rupture parameters of the initial dynamic rupture model based on "Model B" of Ma et al. (2008). Grey dots show 90-day aftershock locations (Neves et al., 2022) projected on the planar fault plane, the black contour indicates the coseismic rupture extent, and the star marks the hypocenter. (a) Moment release rate and moment magnitude. (b) Coseismic slip. (c) Stress drop. (d) Local rupture speed and rupture front contours every 1 s. (e) Peak slip rate. (f) Rise time.

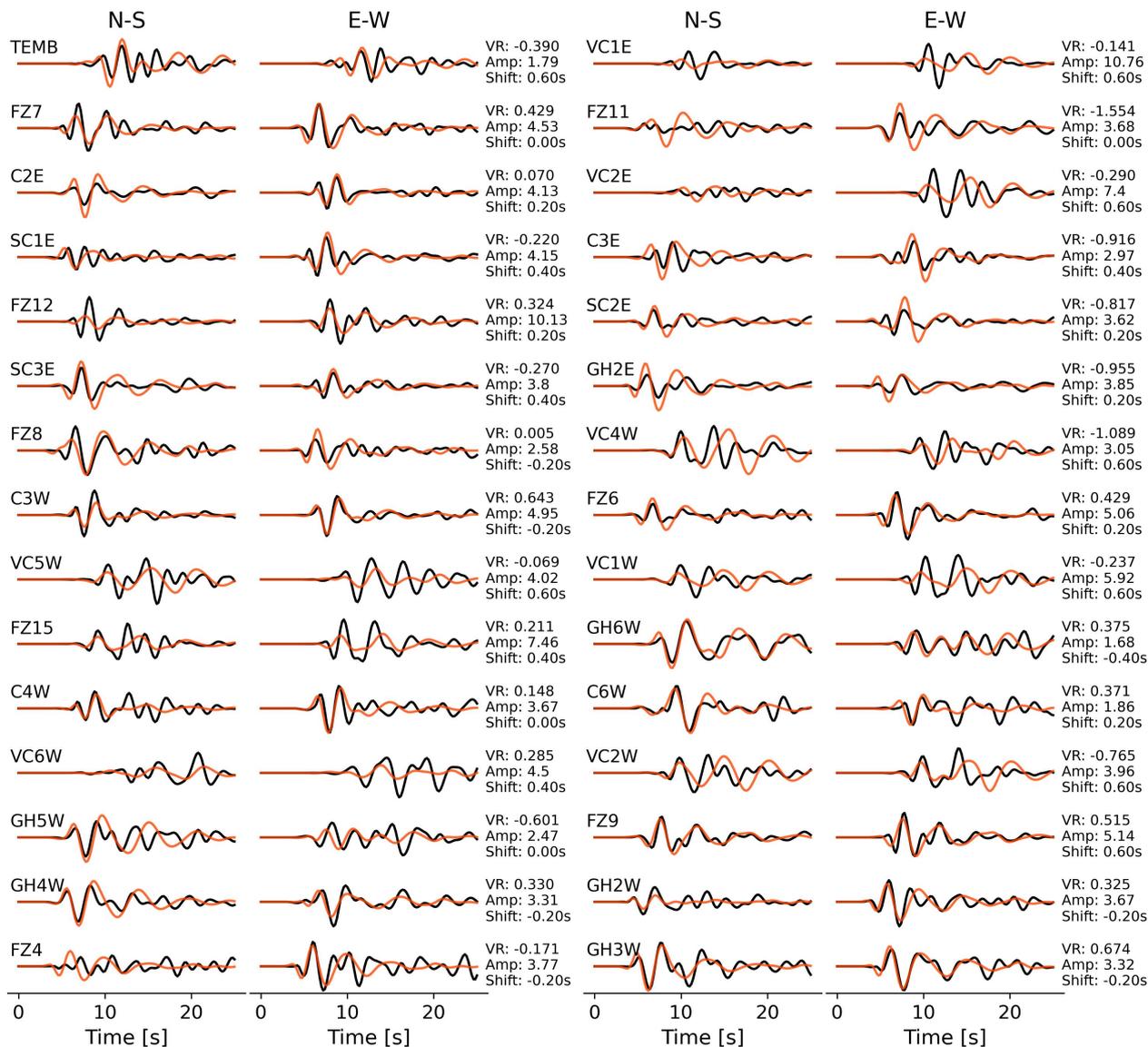


Figure S3. Observed (black) and synthetic (orange) seismic velocity waveforms from the initial dynamic rupture model based on "Model B" of Ma et al. (2008), bandpass filtered between 0.16–0.5 Hz at the 30 stations used to constrain the inversion. Each waveform (synthetic and observed) is normalized by the respective station's maximum amplitude (Amp, in cm/s, either synthetic or observed maximum). The observed waveforms at each station are cross-correlated and time-shifted relative to the synthetics to maximize the variance reduction (VR) and to account for unmodeled effects of topography and the 3D velocity structure.

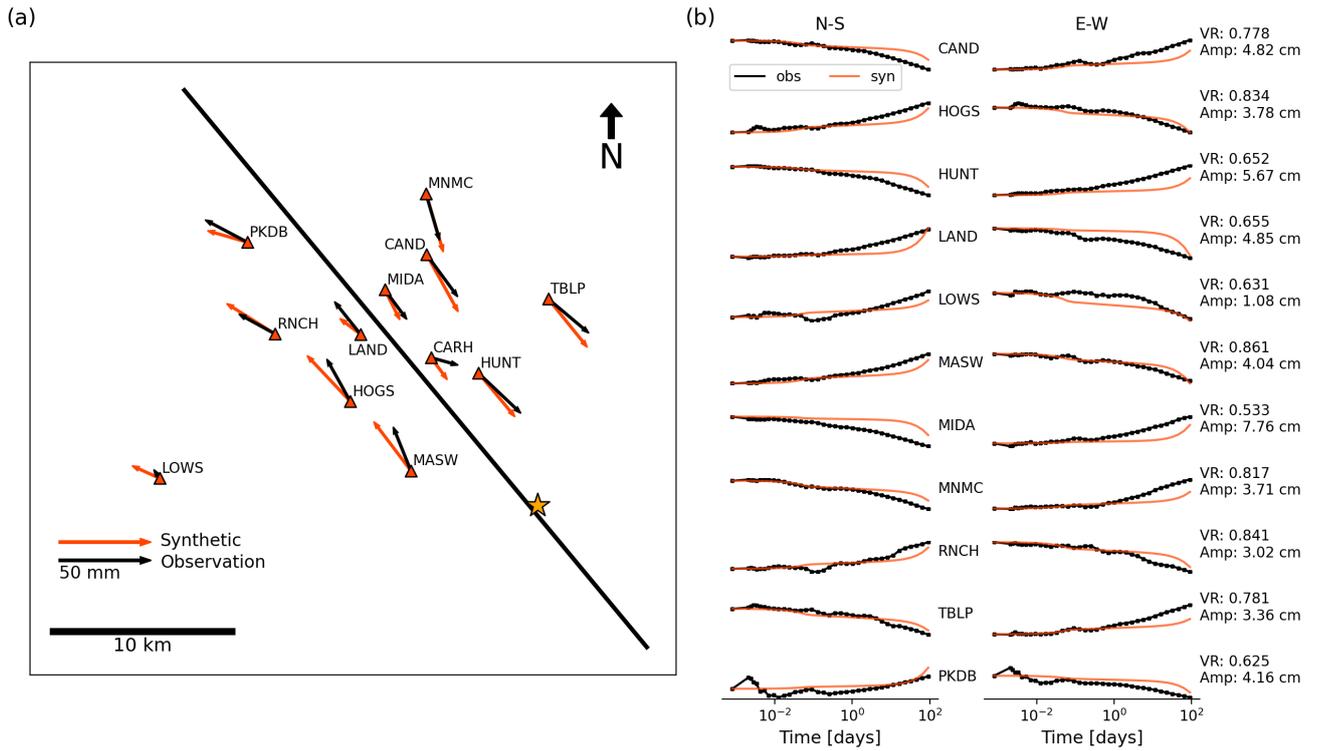


Figure S4. (a) Coseismic horizontal static displacements at 12 GPS stations. Black and orange arrows show observed (Jiang et al., 2021) and synthetic displacements from the initial dynamic rupture model based on "Model B" of Ma et al. (2008), respectively. The black line indicates the fault trace, and the star marks the epicenter. Both synthetic and observed coseismic displacements are given at 90 s after the rupture onset. (b) Postseismic evolution of the normalized displacements at 11 GPS stations (excluding station CARH) during the first 90 days following the earthquake. Black curves show observations (Jiang et al., 2021), and orange curves show the synthetics of our initial model. The time scale is logarithmic. For each station, we annotate its variance reduction inferred after removing the coseismic displacement and its maximum amplitude.

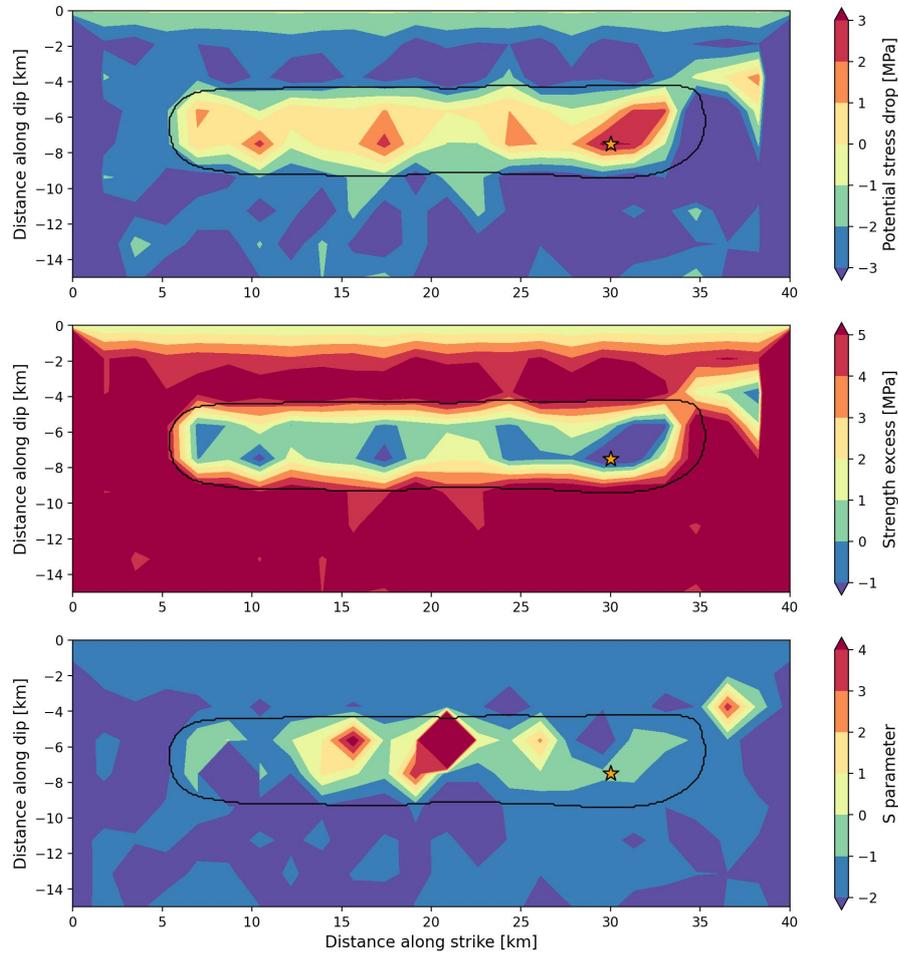


Figure S5. Derived quantities from the dynamic parameters of the initial dynamic rupture model based on "Model B" of Ma et al. (2008). The black contour indicates the coseismic rupture extent, and the star marks the hypocenter. (a) Potential stress drop ($\tau_0 - f_w \sigma_n$). (b) Strength excess ($f_0 \sigma_n - \tau_0$). (c) S parameter ($\frac{\tau^y - \tau^0}{\tau^0 - \tau^d}$).

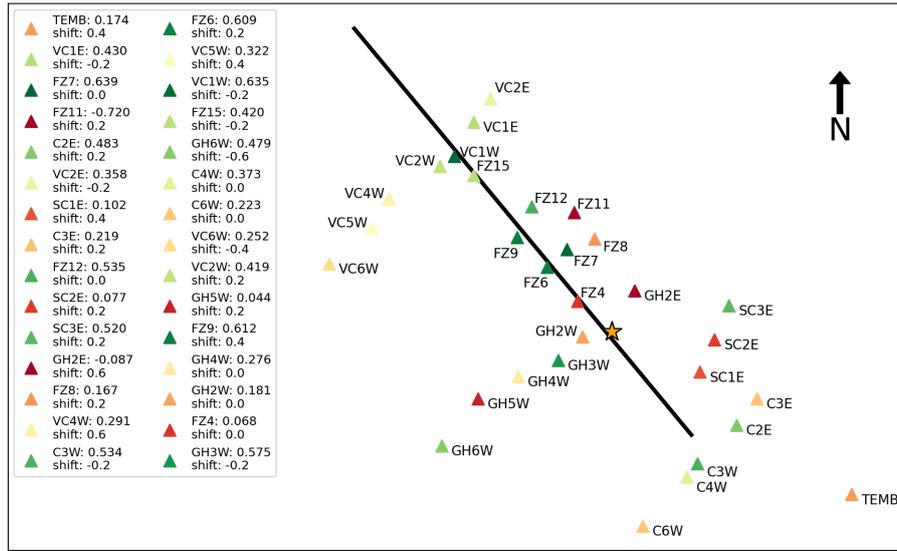


Figure S6. Stations used for constraining the inversion colored by their seismic variance reductions obtained from the preferred joint dynamic rupture and afterslip model. The star marks the epicenter and the black line shows the fault trace of our model’s planar fault.

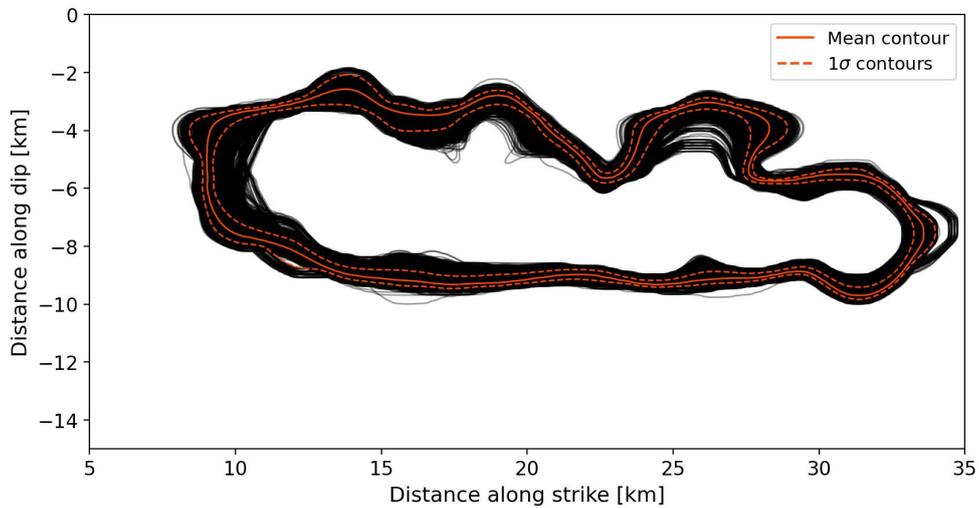


Figure S7. Dynamic rupture extent contours of the 10500 models of the best-fitting ensemble. Orange and dashed orange lines show the mean rupture edge and one standard deviation in both directions, respectively.

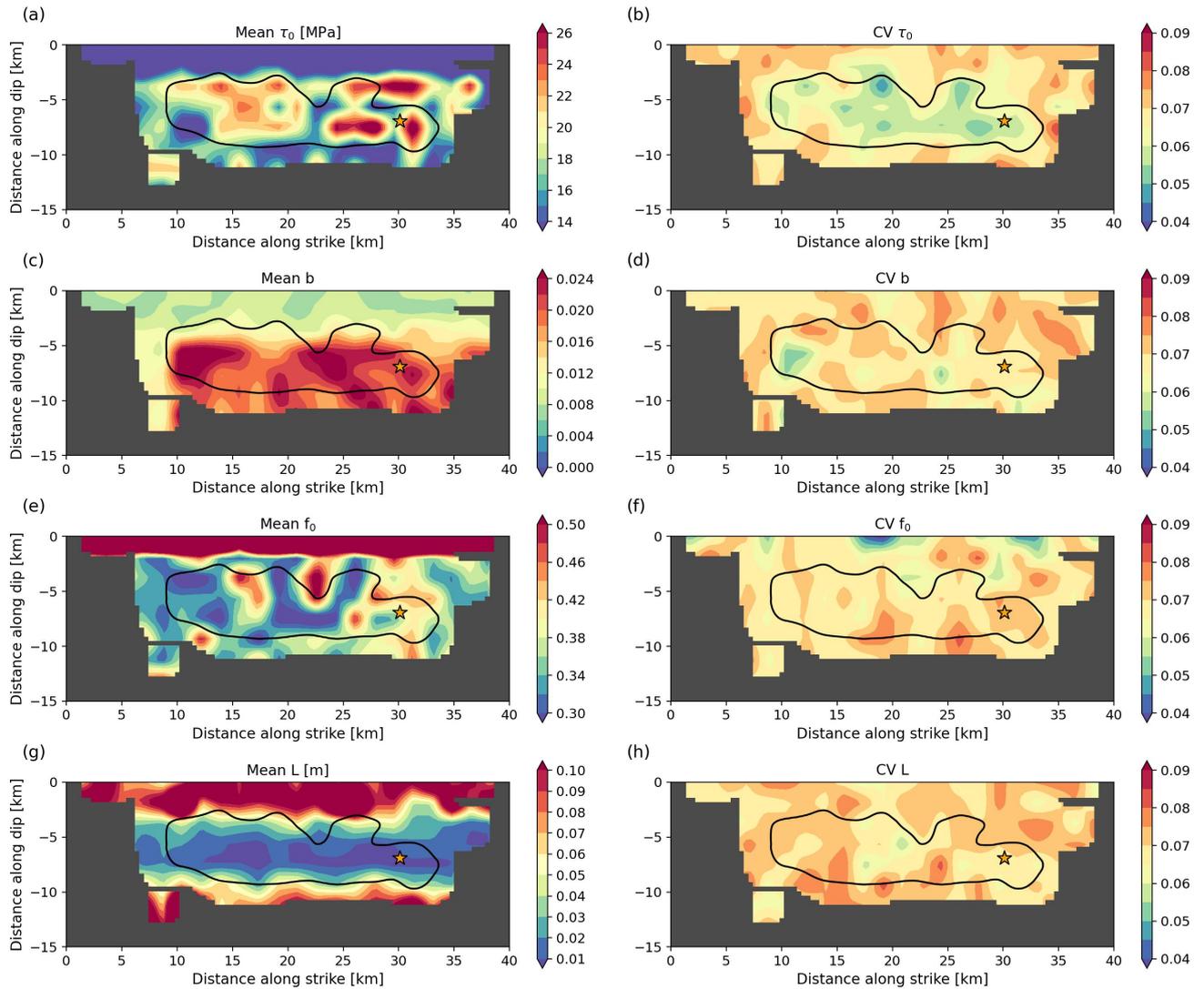


Figure S8. Mean distributions of the best-fitting model ensemble's (a) prestress τ_0 , (c) $b-a$, (e) friction drop $f_0 - f_w$, (g) characteristic weakening distance L , and their corresponding coefficients of variation CV (b,d,f,h). The model ensemble contains 10500 models. We mask areas where the sum of coseismic and postseismic slip does not exceed 10 cm within 1.2 km, which we consider unconstrained.

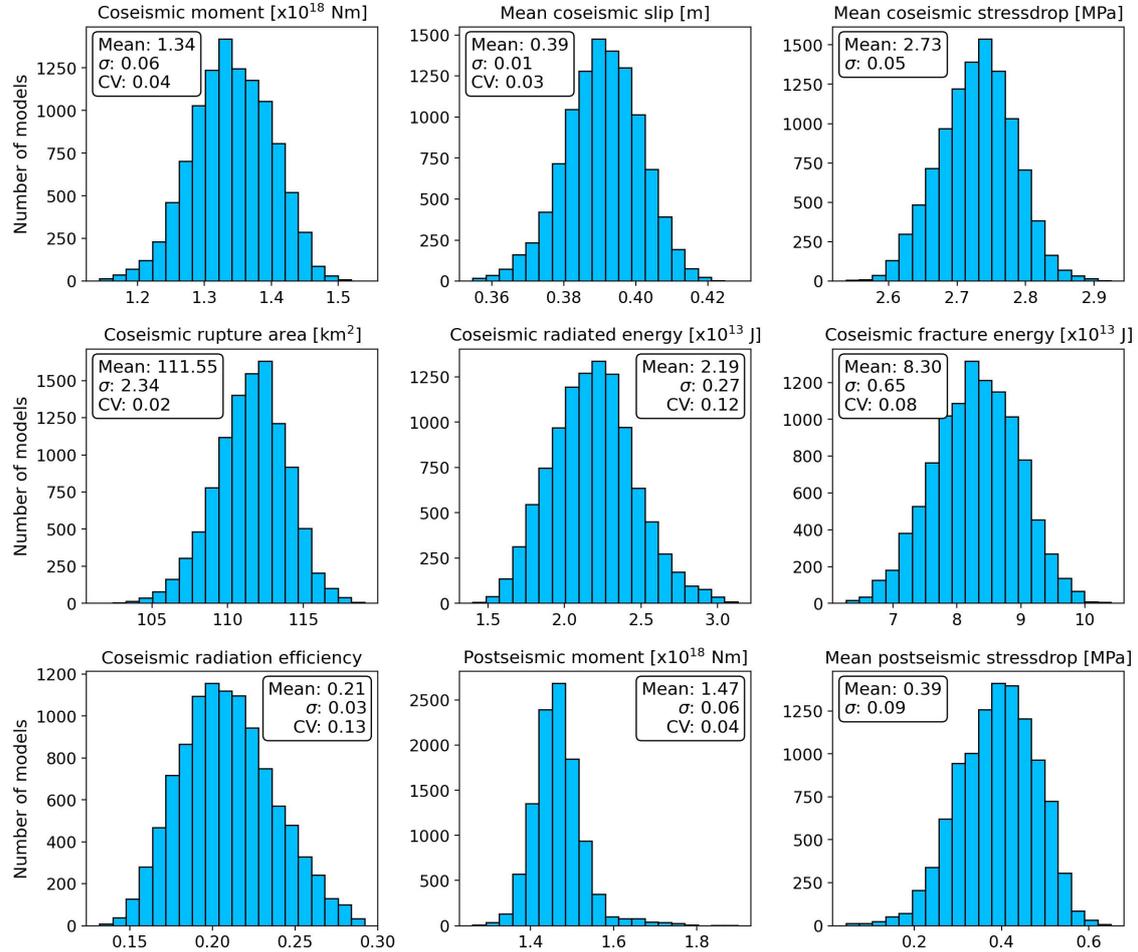


Figure S9. Histograms of various coseismic and postseismic rupture parameters of the best-fitting model ensemble containing 10500 unique joint dynamic rupture and afterslip models. Legends of each subplot show mean values, standard deviations σ , and coefficients of variation CV (ratio of the standard deviation to the mean) for quantities with an absolute zero.

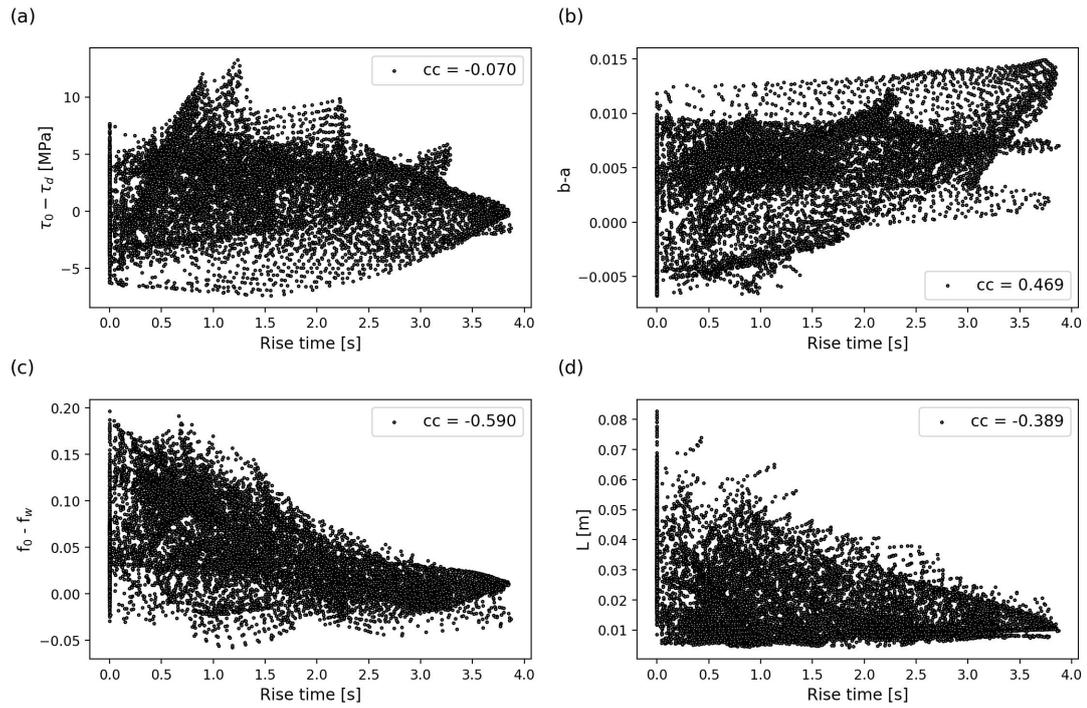


Figure S10. Rise times of each grid point of the preferred joint dynamic rupture and afterslip model plotted against (a) τ_0 , (b) $b - a$, (c), $f_0 - f_w$, (d) L . Subplot legends show correlation coefficients between both variables.

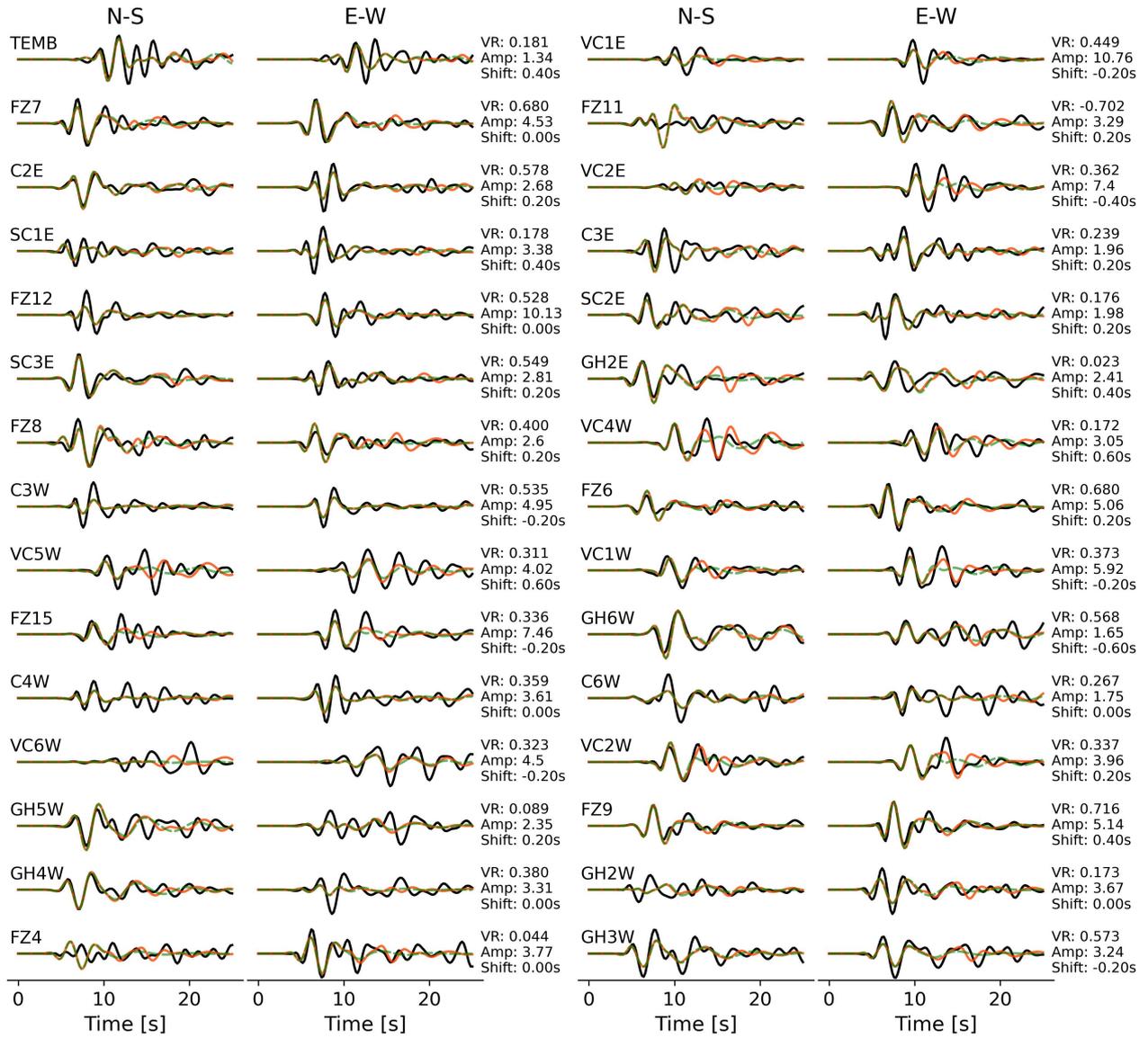


Figure S11. Observed (black) and synthetic (dashed green) velocity waveforms from a **5 s version** of the preferred joint dynamic rupture and afterslip model (including only the initial pulse-like rupture phase) filtered between 0.16 and 0.5 Hz at the 30 stations used to constrain the inversion. The reference model's waveforms (21 s simulation duration) are shown in orange. Each waveform is normalized by the respective station's maximum amplitude (Amp in cm/s). The variance reductions (VR) of the 5 s version are annotated. The observed waveforms at each station are shifted relative to the reference synthetics to account for the effects of topography and the 3D velocity structure by maximizing the VR.

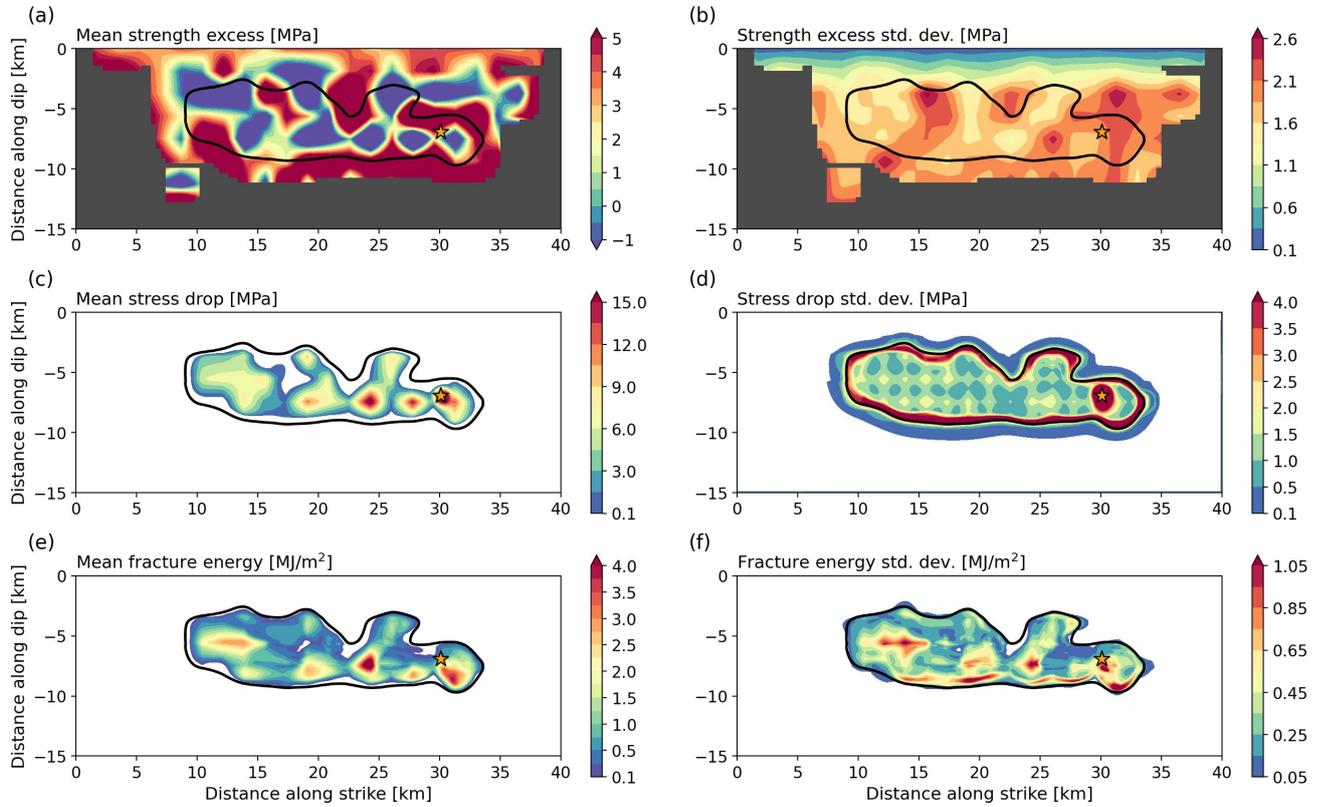


Figure S12. Means of the best-fitting model ensemble's (a) initial strength excess ($f_0\sigma_n - \tau_0$), (c) coseismic stress drop (e) coseismic fracture energy distributions, and the corresponding standard deviations (b,d,f). The model ensemble contains 10500 models. We only show the strength excess where coseismic and postseismic slip combined exceed 10 cm somewhere within a radius of 1.2 km, which we consider as constrained by the inversion.

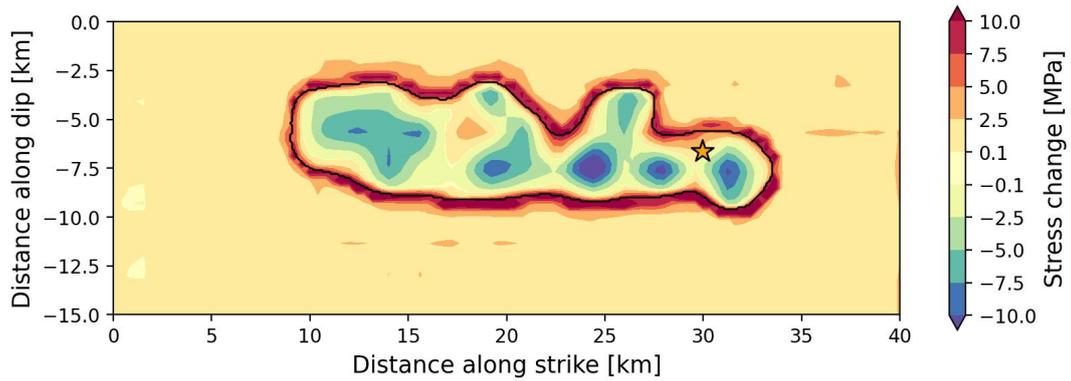


Figure S13. Coseismic stress change of the preferred joint dynamic rupture and afterslip model. The black line indicates the coseismic rupture extent and the star marks the hypocenter.

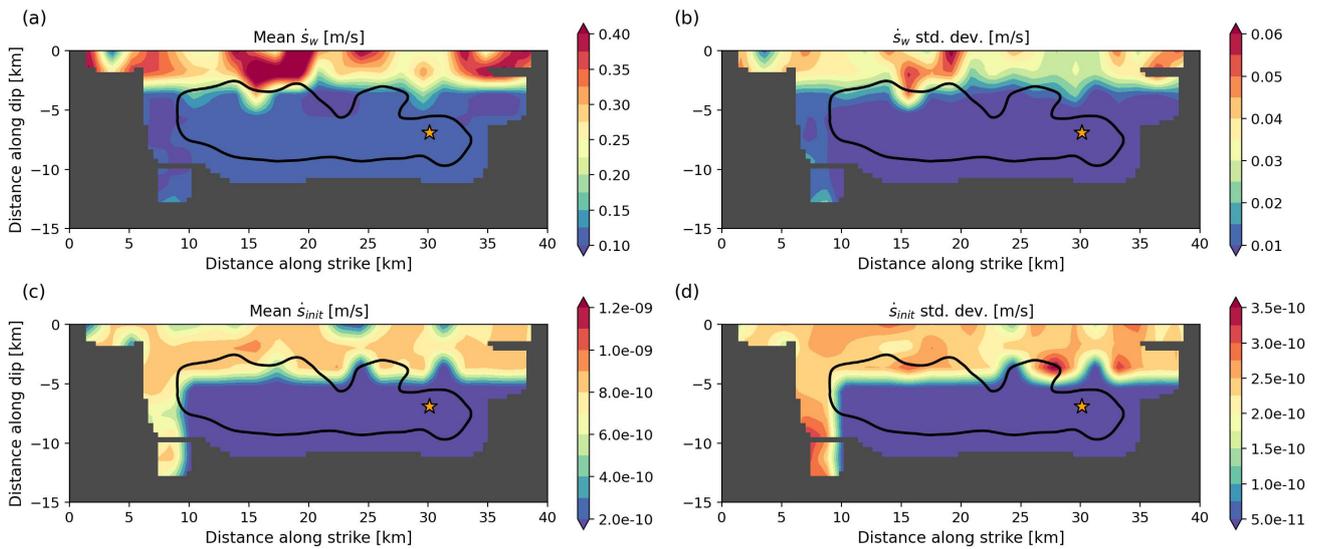


Figure S14. Mean distributions of the best-fitting model ensemble's (a) weakening slip rate \dot{s}_w , (c) initial slip rate \dot{s}_{init} , and the corresponding standard deviations (b,d). The model ensemble contains 10500 models. We hide areas where the sum of coseismic and postseismic slip does not exceed 10 cm within 1.2 km, which we consider unconstrained.

Table S1. 1D velocity profiles on the southwest and northeast side of the fault (Custódio et al., 2005) used to calculate the Green’s functions. The dynamic rupture solver uses the average velocity profile. Q values are based on v_s : $Q_s = 0.1 v_s$ (in m/s) and $Q_p = 1.5 Q_s$ (Olsen et al., 2003).

Lower extent [km]	v_p [m/s]	v_s [m/s]	Density [kg/m ³]	Q_p	Q_s
southwest					
1.0	2000	1100	2000	165	110
2.0	3500	2000	2300	300	200
3.0	4500	2500	2300	375	250
3.5	5200	3000	2500	450	300
5.8	5700	3200	2700	480	320
14.1	6200	3600	2700	540	360
17.1	6800	3600	2800	540	360
20.4	6800	4300	2800	645	430
∞	7300	4300	2800	645	430
northeast					
1.0	2000	1100	2000	165	110
1.8	3500	2200	2300	330	220
2.1	4200	2800	2300	420	280
3.4	4800	2700	2300	405	270
3.9	5200	2800	2300	420	280
8.3	5300	3200	2700	480	320
12.7	5700	3700	2800	555	370
17.5	6500	3800	2800	570	380
20.3	6700	4300	2800	645	430
∞	7300	4300	2800	645	430
average					
1.0	2000	1100	2000	165	110
2.0	3500	2100	2300	315	210
3.5	4400	2700	2300	405	270
5.8	5500	3000	2500	450	300
12.7	5800	3600	2700	540	360
17.1	6500	3800	2800	570	380
20.3	6800	4300	2800	645	430
∞	7300	4300	2800	645	430

Table S2. Step size ranges of the model parameter perturbations during the inversion. The parameter perturbations are drawn from a log-normal distribution and the step size represents its relative standard deviation. The step size is successively reduced to keep the model acceptance rate reasonable.

Label	Parameters	Log-normal step size (in %)
τ_0	Shear prestress	0.3–2.0
b	state evolution parameter	0.3–2.0
f_0	Reference friction coefficient at $\dot{s}_0 = 10^{-6}$	0.3–2.0
L	Characteristic slip distance	0.3–2.0
\dot{s}_w	Weakening slip rate	0.3–2.0
\dot{s}_{init}	Initial slip rate	2.0
h_x	Along-strike position of nucleation patch	0.3–2.0
h_z	Along-dip position of nucleation patch	0.3–2.0
r_{nuc}	Radius of the nucleation patch	0.3–2.0
σ_{nuc}	Stress increase within the nucleation patch	0.3–2.0

References

- Custódio, S., Liu, P., & Archuleta, R. J. (2005). The 2004 Mw6.0 Parkfield, California, earthquake: Inversion of near-source ground motion using multiple data sets. *Geophysical Research Letters*, *32*.
- Jiang, J., Bock, Y., & Klein, E. (2021). Coevolving early afterslip and aftershock signatures of a San Andreas fault rupture. *Science Advances*, *7*.
- Ma, S., Custódio, S., Archuleta, R. J., & Liu, P. (2008). Dynamic modeling of the 2004 Mw 6.0 Parkfield, California, earthquake. *Journal of Geophysical Research: Solid Earth*, *113*.
- Neves, M., Peng, Z., & Lin, G. (2022). A High-Resolution Earthquake Catalog for the 2004 Mw 6 Parkfield Earthquake Sequence Using a Matched Filter Technique. *Seismological Research Letters*, *94*.
- Olsen, K. B., Day, S. M., & Bradley, C. R. (2003). Estimation of Q for Long-Period (>2 sec) Waves in the Los Angeles Basin. *Bulletin of the Seismological Society of America*, *93*.